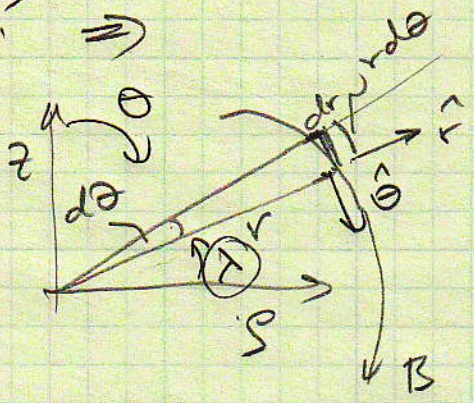


① $\vec{B} = B_0 \left(\frac{R}{r}\right)^3 (2 \cos \theta \hat{r} + \sin \theta \hat{\theta})$

a)



$$\frac{dr}{r d\theta} = \frac{B_r}{B_\theta} = \frac{2 \cos \theta}{\sin \theta}$$

$$\frac{dr}{r} = \frac{2 \cos \theta}{\sin \theta} d\theta$$

$$\ln r = 2 \ln \sin \theta + \text{const}$$

B.C. $r = R @ \theta = \pi/2$

$$r = R \sin^2 \theta$$

or $r = R \cos^2 \lambda$

$$R_c = \frac{(r^2 + v_\lambda^2)^{3/2}}{|r^2 + 2r_\lambda^2 - r r_{\lambda\lambda}|}$$

$$\Rightarrow \frac{R^3}{R^2 + 2R^2} = \underline{\underline{\frac{R}{3}}}$$

$$r_\lambda = \frac{dr}{d\lambda} = -2R \cos \lambda \sin \lambda$$

$$\Rightarrow \left. \begin{array}{l} \lambda = 0 \\ r_\lambda = 0 \end{array} \right\}$$

$$r_{\lambda\lambda} = \frac{d^2r}{d\lambda^2} = -2R(\cos^2 \lambda - \sin^2 \lambda) \Rightarrow -2R$$

$$\Rightarrow -2R$$

b) curvature and gradient drift

drift energy = $w_{||} + w_{\perp}$
@ $\lambda = 0$

$$\vec{V}_c = \frac{2w_{||}}{qB} \left[\frac{\hat{B} \times \hat{R}_c}{R_c} \right]$$

$$\vec{V}_c = \frac{6w_{||}}{qB R} \hat{\phi}$$

$$\vec{V}_G = \frac{\omega_{\perp}}{qB} \left[\frac{\hat{B} \times \nabla B}{B} \right]$$

$$\nabla B = \nabla \left[B_0 \left(\frac{R_p}{r} \right)^3 \right] \Rightarrow -3 B_0 \frac{R_p^3}{r^4} \hat{r} = -3B \frac{\hat{r}}{r}$$

$$\boxed{\vec{V}_G = \frac{3 \omega_{\perp}}{qB} \frac{1}{R} \hat{\phi}}$$

e) pitch angle $\pi/2 \Rightarrow \omega_{\parallel} = 0$

$$\vec{V}_{\text{drift}} = \vec{V}_G$$

Energy $\omega_{\perp} = 10^3 \text{ eV} \Rightarrow 1.6 \times 10^{-16} \text{ J (Nm)}$
 (pitch an energy)

$$R = R_{\text{synch}} = 6.68 R_E =$$

$$R_E = 6378 \text{ km} \approx 6.4 \times 10^6 \text{ m}$$

$$q = 1.6 \times 10^{-19} \text{ C}$$

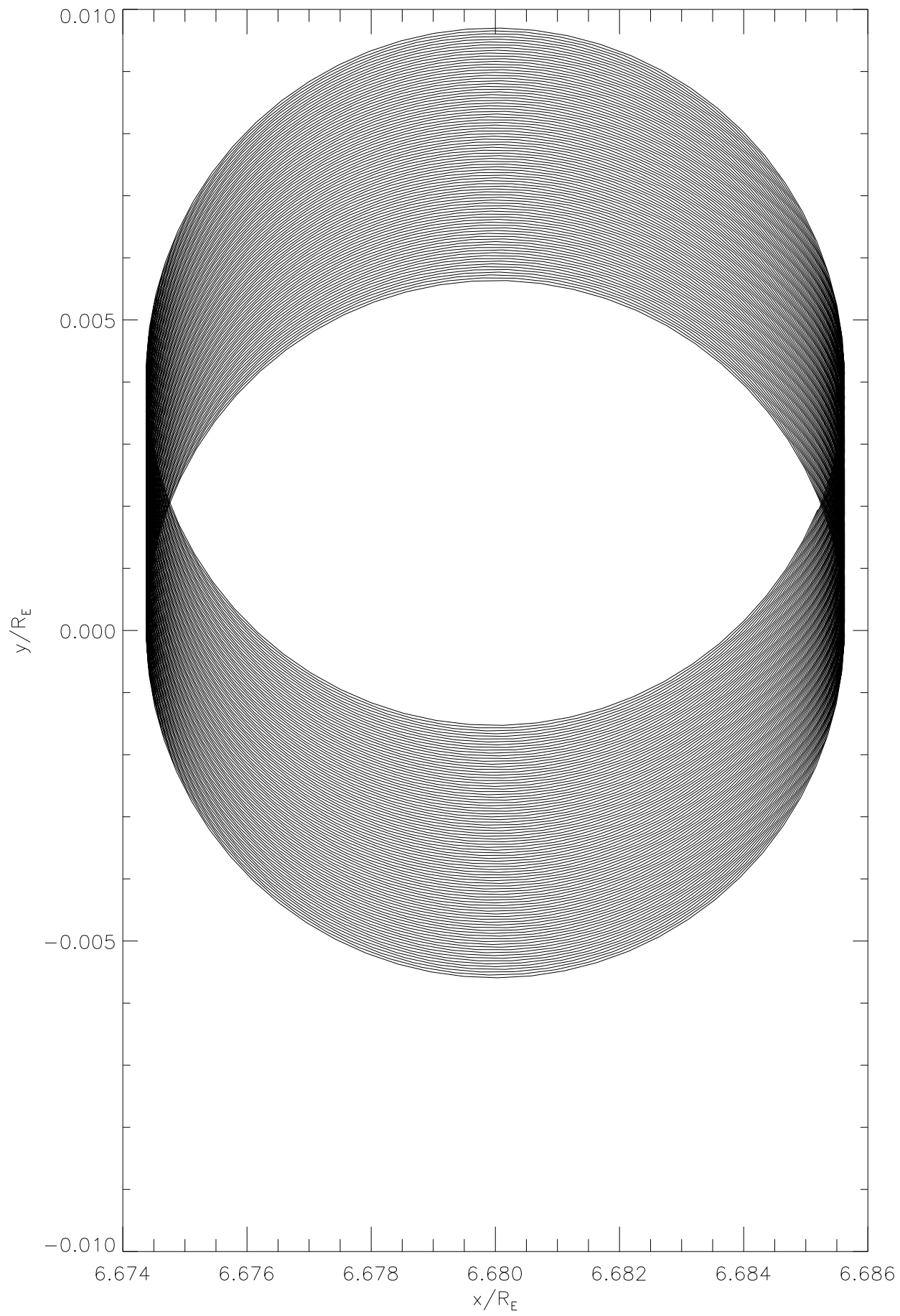
$$B_0 = 30 \times 10^{-6} \text{ T} \Rightarrow B = \frac{B_0}{(6.68)^3} \approx 10^{-7} \text{ Tesla}$$

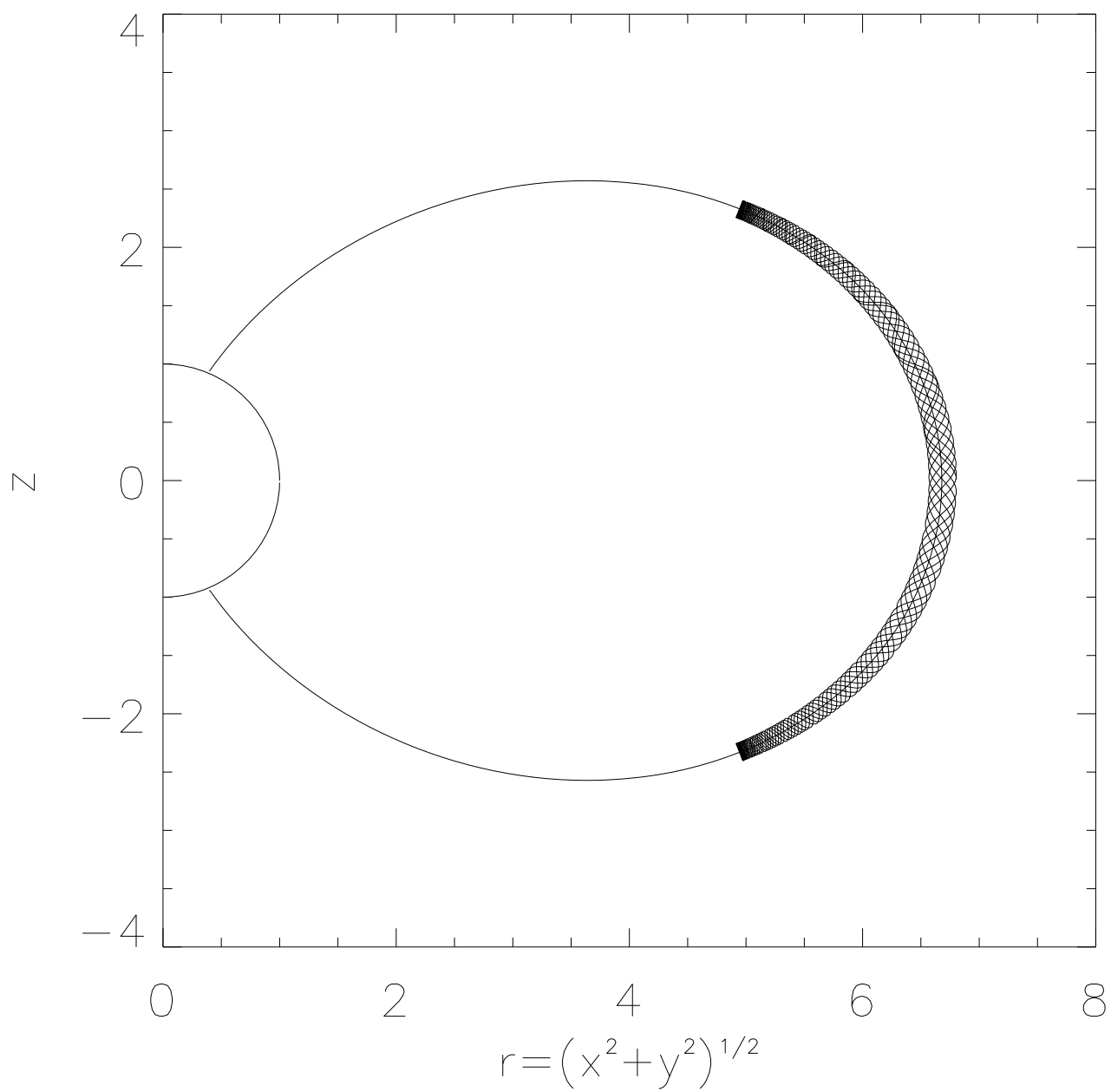
$$\vec{V}_G = \frac{3 \times 1.6 \times 10^{-16}}{1.6 \times 10^{-19} \cdot 10^{-7}} \frac{1}{(6.68 \times 6.4 \times 10^6)} \text{ m/s}$$

$$\vec{V}_G \approx 700 \text{ m/s} \approx 0.7 \text{ km/s}$$

from the code $\vec{V}_{\text{numerical}} \approx \frac{0.005 R_E}{60 \text{ sec}} \approx 560 \text{ m/s}$

d) attached for $KE = 10^6 \text{ eV}$ $\alpha_{\text{pitch}} = \pi/4$





Contributors

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```

=====
c (in this code cgs units are used )
c
=====
c earth.f
c PHYS 5150 Spring, 2009

implicit real*8 (a-h,o-z)
dimension ff(6)
common /params/ B_0,pm,q,r_e,dpm,c,pi
real L, L_m, L_p, L_pp
external diff
logical OK

call startup
c initial conditions
L=6.68
x=r_e*L
y=0.
z=0.
c energy KE = 1.e6 ev
xe=1.e6*1.e-12
v=sqrt(2*xe/pm)
c mirror latitude
L_m=20.*pi/180.
c B at the equator
B_e=B_0/L**3

c pitch angle L_p
L_p=pi/4.
Mihaly Hor...
Mihaly...
vx=0.
vy=v*sin(L_p)
vz=v*cos(L_p)
c Larmor radius
r_L=pm*vy*c/(q*B_e)
x=x+r_L
c integrator settings:
n=6
acc=1.e-12
h=1.e-1
hmin=1.e-13
jtest=0

ff(1)=x
ff(2)=y
ff(3)=z
ff(4)=vx
ff(5)=vy
ff(6)=vz
t1=0.
dt=1.e-2

do 100 i=1,100*60
t2=t1+dt
c to avoid crash

```

```

      r1=sqrt(ff(1)**2+ff(2)**2+ff(3)**2)
      if(r1.le.r_e) go to 1000
c integration begins
      call merson(t1,t2,ff,6,acc,h,hmin,jtest,OK,diff)

      t1=t2
      r=sqrt(ff(1)**2+ff(2)**2)/r_e
      xre=ff(1)/r_e
      yre=ff(2)/r_e
      zre=ff(3)/r_e
      write(8,66),t1,xre,yre,zre,ff(4)/1.e5,ff(5)/1.e5,ff(6)/1.e5

66  format(7e15.7)
100  continue

1000 continue

      stop
      end

cccccccccccccccccccc

      subroutine startup
      implicit real*8 (a-h,o-z)
      common /params/ B_0,pm,q,r_e,dpm,c,pi

c proton
      pm=1.6726e-24
      q=4.8e-10

C Earth
      r_e=6384.4e5
      B_0=0.3
      dpm=B_0*r_e**3
c   print*,'dpm=',dpm

c speed of light
      c=3.e10
      pi=acos(-1.)
      return
      end

      subroutine diff(t,ff,ffp)
      implicit real*8 (a-h,o-z)
      common /params/ B_0,pm,q,r_e,dpm,c,pi
      common /force/ flx,fly,flz
      dimension ff(6), ffp(6)

      x=ff(1)
      y=ff(2)
      z=ff(3)
      vx=ff(4)
      vy=ff(5)
      vz=ff(6)
      call forces(x,y,z,vx,vy,vz,fx,fy,fz)
      ffp(1)=vx
      ffp(2)=vy
      ffp(3)=vz
      ffp(4)=fx/pm
      ffp(5)=fy/pm
      ffp(6)=fz/pm

      return
      end

      subroutine forces(x,y,z,vx,vy,vz,fxl,fyl,fzl)

```

```

      implicit real*8 (a-h,o-z)
      common /params/ B_0,pm,q,r_e,dpm,c,pi

      call fields(x,y,z,bx,by,bz)
c Lorentz force
      fxl=q*(vy*bz-vz*by)/c
      fyl=q*(vz*bx-vx*bz)/c
      fzl=q*(vx*by-vy*bx)/c

      return
      end

      subroutine fields(x,y,z,bx,by,bz)
      implicit real*8 (a-h,o-z)

      common /params/ B_0,pm,q,r_e,dpm,c,pi

c aligned, centered dipole
      r2=x**2+y**2+z**2
      r=sqrt(r2)
      r3=r**3
      bx=3.*x/r3*z*dpm/r2
      by=3.*y/r3*z*dpm/r2
      bz=(3.*z*z/r2-1.)*dpm/r3

      return
      end

      SUBROUTINE MERSON (X,XEND,Y,N,ACC,H,HMIN,JTEST,OK,DIFF)
      implicit real*8 (a-h,o-z)

c this is a nice integrator, one can force integration forward even
c if the requested accuracy is not achieved
c
C   CERN LIBRARY NO D 208.
C
C   REVISED VERSION JULY 1971.
C
C   THIS VERSION OF MERSON IS A MODIFICATION OF THE PROGRAM RECEIVED
C   FROM KJELLER COMPUTER INSTALLATION NORWAY.THE MAIN DIFFERENCE
C   BEEING A CHANGE OF THE TEST FOR STEPLENGTH HALVING.
C
C
C   PURPOSE = STEP BY STEP INTEGRATION OF A SYSTEM OF FIRST ORDER
C             DIFFERENTIAL EQUATIONS
C
C             DYK(X)/DX=FK(X,Y1(X),Y2(X),.....,YN(X)) , K=1(1)N
C
C             WITH AUTOMATIC ERROR CONTROL USING THE METHOD DUE TO
C             MERSON.
C
C   PARAMETERS
C
C   X       = START VALUE FOR THE DOMAIN OF INTEGRATION (INPUT POINT).
C   XEND    = END VALUE FOR THE DOMAIN OF INTEGRATION (OUTPUT POINT).
C   Y       = ARRAY CONTAINING THE DEPENDENT VARIABLES.WHEN ENTERING
C             THE ROUTINE THE FUNCTION VALUES YK(X),K=1(1)N AND WHEN
C             RETURNING TO THE CALLING PROGRAM THE COMPUTED FUNCTION
C             VALUES YK(XEND),K=1(1)N.
C   N       = THE NUMBER OF DIFFERENTIAL EQUATION,EQUAL OR LESS 100.
C   ACC     = PRESCRIBED RELATIVE ACCURACY (TO BE OBTAINED FOR ALL
C             FUNCTION VALUES IN THE ARRAY Y).
C   H       = INITIAL STEPLENGTH.
C   HMIN    = ABSOLUTE VALUE OF MINIMUM STEPLENGTH WANTED.
C   JTEST   = TEST PARAMETER RELATED TO THE STEPLENGTH IN THE FOLLOW-

```

```

C          ING WAY.
C          JTEST = 0 , IF DURING THE CALCULATION WE GET
C          ABS(H).LT.HMIN (BY REPEATED HALVING OF THE
C          STEPLENGTH), THEN AN ERROR MESSAGE IS PRINT-
C          ED, OK SET EQUAL TO .FALSE. FOLLOWED BY RE-
C          TURN TO THE CALLING PROGRAM.
C          JTEST = 1 , CHECKING AS FOR JTEST=0, BUT THE CALCULATION
C          WILL CONTINUE WITH THE FIXED STEPLENGTH HMIN
C      OK    = A LOGICAL VARIABLE WHICH IS SET EQUAL TO .TRUE. WHEN EN-
C          TERING THE ROUTINE. THE VALUE LATER IS DEPENDING OF JTEST
C          IN THE FOLLOWING WAY
C          JTEST = 1 , OK = .TRUE. ALWAYS.
C          JTEST = 0 , OK = .FALSE. IF THE STEPLENGTH BECOMES TOO
C          SMALL (SEE DESCRIPTION FOR JTEST).
C      DIFF  = USER SUPPLIED SUBROUTINE FOR THE CALCULATION OF THE
C          RIGHT HAND SIDES OF THE SYSTEM OF DIFFERENTIAL EQUATIONS
C          (I.E. THE FIRST ORDER DERIVATIVES). CALLING SEQUENCE
C          CALL DIFF(X,W,F) , WHERE
C          X = THE CURRENT VALUE OF THE ARGUMENT
C          W = AN ARRAY WITH THE ELEMENTS WK(X), K=1(1)N I.E. THE
C          FUNTION VALUES FOR WHICH THE DERIVATIVES ARE TO BE
C          COMPUTED.
C          F = AN ARRAY WITH THE ELEMENTS FK(X), K=1(1)N (WE HAVE
C          FK(X)=FK(X,W1(X),W2(X),...,WN(X))) TO BE COMPUTED
C          BY DIFF AND RETURNED TO MERSON.
C          THE CHOSEN NAME FOR DIFF MUST APPEAR IN AN EXTERNAL
C          STATEMENT IN THE PROGRAM CALLING MERSON.
C
C      THE ARRAYS IN THE COMMON BLOCK BELOW ARE ONLY USED INTERNALLY IN
C      MERSON (AND DIFF) AND ARE TO FREE DISPOSAL OUTSIDE MERSON.
C      THE MAXIMUM NUMBER OF EQUATIONS WHICH MAY BE INTEGRATED ARE 100.
C      THIS NUMBER MAY BE CHANGED BY CHANGING THE DIMENSION IN THE
C      COMMON BLOCK BELOW ACCORDINGLY.
C
C      COMMON / LOCAL / YZ(100) , A(100) , B(100) , F(100) , W(100)
C
C      LOGICAL OK
C      DIMENSION Y(N)
C
C      RZERO IS A NUMBER WITH A MAGNITUDE OF ORDER EQUAL TO THE NOISE
C      LEVEL OF THE MACHINE I.E. IN THE RANGE OF THE ROUNDING OFF ERRORS.
C
C      DATA RZERO / 1.E-13 /
C
C      CHECK NUMBER OF EQUATIONS, EQUAL OR LESS THAN 100.
C
C      IF (N.GT.100) GO TO 86
C
C      OK=.TRUE.
C
C      STORE INTERNALLY PARAMETERS IN LIST
C
C      NN=N
C      DO 1 K=1,NN
1  W(K)=Y(K)
C      Z=X
C      ZEND=XEND
C      BCC=ACC
C      ZMIN=HMIN
C      ITEST=JTEST
C      S =H
C      ISWH=0
C
C      2 HSV=S
C      COF=ZEND-Z
C      IF (ABS(S).LT.ABS(COF)) GO TO 8
C      S=COF
C      IF (ABS(COF/HSV).LT.RZERO) GO TO 50

```



```

      ISWH=1
C
C   IF ISWH=1 THEN S IS EQUAL TO MAXIMUM POSSIBLE STEPLENGTH
C   WITHIN THE REMAINING PART OF THE DOMAIN OF INTEGRATION.
C
      8 DO 10 K=1,NN
      10 YZ(K)=W(K)
      12 HT=.333333333333333*S
C
      CALL DIFF(Z,W,F)
C
      Z=Z+HT
      DO 20 K=1,NN
      A(K)=HT*F(K)
      20 W(K)=A(K)+YZ(K)
C
      CALL DIFF(Z,W,F)
C
      DO 22 K=1,NN
      A(K)=.5*A(K)
      22 W(K)=.5*HT*F(K)+A(K)+YZ(K)
C
      CALL DIFF(Z,W,F)
C
      Z=Z+.5*HT
      DO 24 K=1,NN
      B(K)=4.5*HT*F(K)
      24 W(K)=.25*B(K)+.75*A(K)+YZ(K)
C
      CALL DIFF(Z,W,F)
C
      Z=Z+.5*S
      DO 26 K=1,NN
      A(K)=2.*HT*F(K)+A(K)
      26 W(K)=3.*A(K)-B(K)+YZ(K)
C
      CALL DIFF(Z,W,F)
C
      DO 28 K=1,NN
      B(K)=-.5*HT*F(K)-B(K)+2.*A(K)
      W(K)=W(K)-B(K)
      A(K)=ABS(5.*BCC*W(K))
      B(K)=ABS(B(K))
      IF (ABS(W(K)).LE.RZERO) GO TO 28
      IF (B(K).GT.A(K)) GO TO 60
      28 CONTINUE
C
C   REQUIRED ACCURACY OBTAINED FOR ALL COMPUTED FUNCTION VALUES.
C
      IF (ISWH.EQ.1) GO TO 50
C
C   TEST IF STEPLENGTH DOUBLING IS POSSIBLE.
C
      40 DO 42 K=1,NN
      IF (B(K).GT. .03125*A(K)) GO TO 2
      42 CONTINUE
      S=S+S
      GO TO 2
C
C   CALCULATION FINISHED.REPLACE INPUT FUNCTION VALUES WITH THE FUNC-
C   TION VALUES COMPUTED FOR THE OUTPUT POINT XEND.REPLACE INPUT STEP-
C   LENGTH H WITH NEW COMPUTED STEPLENGTH.
C
      50 H=HSV
      X=Z
      DO 52 K=1,NN
      52 Y(K)=W(K)
C

```

```
      RETURN
C
C   REQUIRED ACCURACY NOT OBTAINED.
C
C
60   COF=.5*S
      IF (ABS(COF).GE.ZMIN) GO TO 80
      IF (ITEST.EQ.0) GO TO 84
C
C   JTEST=1, CONTINUE WITH CONSTANT STEPLENGTH EQUAL HMIN.
C
      S=ZMIN
      IF (HSV.LT.0.) S=-S
      IF (ISWH.EQ.1) GO TO 50
      GO TO 2
C
C   DO CALCULATIONS RELATED TO HALVING OF STEPLENGTH.
C
80   DO 82 K=1, NN
82   W(K)=YZ(K)
      Z=Z-S
      S=COF
      ISWH=0
      GO TO 2
C
C   JTEST=0 AND ABS(S).LT.HMIN.PRINT ERROR MESSAGE, SET OK=.FALSE. AND
C   RETURN TO CALLING PROGRAM.
C
84   PRINT 88 , ITEST , S , ZMIN , Z
      OK=.FALSE.
      GO TO 50
C
86   PRINT 90 , N
      STOP
C
88   FORMAT(//,5X,31H*** SUBROUTINE MERSON ERROR ***,2X,8HJTEST = ,I2,
12X,4HH = ,E12.5,2X,7HMIN = ,E12.5,2X,4HX = ,E12.5,/)
90   FORMAT(//,5X,31H*** SUBROUTINE MERSON ERROR ***,4H N=,I4,1X,55HGR
1EATER THAN THE MAXIMUM NUMBER OF EQUATIONS PERMITTED.,/)
C
      END
C
C
C
C
```

Contributors

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```
pro traj
; IDL routine to plot the trajectory calculated in earth.f
Mihaly Horanyi
L=6.68
lm=(findgen(180)-90)*!pi/180.0
r=L*cos(lm)^2
x=r*cos(lm)
y=r*sin(lm)
ind=where(r gt 1)
set_xy,0,7,-4,4
plot,x(ind),y(ind),/isotropic,xtit='r=(x!e2!n+y!e2!n)!e1/2!n', ytit='z', chars=2

lm=findgen(360)*!Pi/180
x=cos(lm)
y=sin(lm)
oplot,x,y

lm=20*!pi/180.
x=findgen(100)*0.1
y=x*tan(lm)
;oplot,x,y
;oplot,x,-y

lm=40*!pi/180.
x=findgen(100)*0.1
y=x*tan(lm)
;oplot,x,y
;oplot,x,-y

lm=60*!pi/180.
x=findgen(100)*0.1
y=x*tan(lm)
;oplot,x,y
;oplot,x,-y
read7, 'fort.8', t,x,y,z,vx,vy,vz
r=sqrt(x*x+y*y)
en=sqrt(vx*vx+vy*vy+vz*vz)
err=(en-en(0))/en(0)
oplot,r,z

stop
end
```