

# Solar Orbiter EUI

## Extreme UV Imager



# EUI Cleanliness and Calibration Concepts

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## → SOLAR ORBITER FACTSHEET

### → MISSION

To study the Sun up close and from **high latitudes**, providing the **first images** of the **Sun's poles** and investigating the **heliosphere**

### → PARTNERSHIPS



Solar Orbiter is an **ESA** mission with strong **NASA** participation

### → SPACECRAFT

Launch mass: **1800 kg**  
 Science payload mass: **209 kg**  
 Body: **2.5 m x 3.1 m x 2.7 m**  
 Total length with solar arrays deployed: **18 m**  
 Solar panels: **6, each 2.1 x 1.2 m**  
 Payload power: **180 W**  
 Instrument boom: **4.4 m**  
 3 x radio and plasma waves antennas: **6.5 m each**

### → JOURNEY TO SPACE



Multiple **gravity assists with Venus** will increase Solar Orbiter's inclination out of the plane of the Solar System by 24° (nominal mission) to 33° (extended mission)



### → SCIENCE INSTRUMENTS

#### EPD: Energetic Particle Detector

PI: Javier Rodríguez-Pacheco, University of Alcalá, Spain

#### EUI: Extreme Ultraviolet Imager

PI: Pierre Rochus, Centre Spatial de Liège, Belgium

#### MAG: Magnetometer

PI: Tim Horbury, Imperial College London, UK

#### Metis: Coronagraph

PI: Marco Romoli, INAF – University of Florence, Italy

#### PHI: Polarimetric and Helioseismic Imager

PI: Sami Solanki, Max-Planck-Institut für Sonnensystemforschung, Germany

#### RPW: Radio and Plasma Waves

PI: Milan Maksimovic, LESIA, Observatoire de Paris, France

#### SoloHI: Heliospheric Imager

PI: Russell A. Howard, US Naval Research Laboratory, Washington, D.C., USA

#### SPICE: Spectral Imaging of the Coronal Environment

European-led facility instrument  
 Operations PI: Frédéric Auchère, Institut d'Astrophysique Spatiale, Orsay, France

#### STIX: X-ray Spectrometer/Telescope

PI: Säm Krucker, FHNW, Windisch, Switzerland

#### SWA: Solar Wind Plasma Analyser

PI: Christopher Owen, Mullard Space Science Laboratory, UK

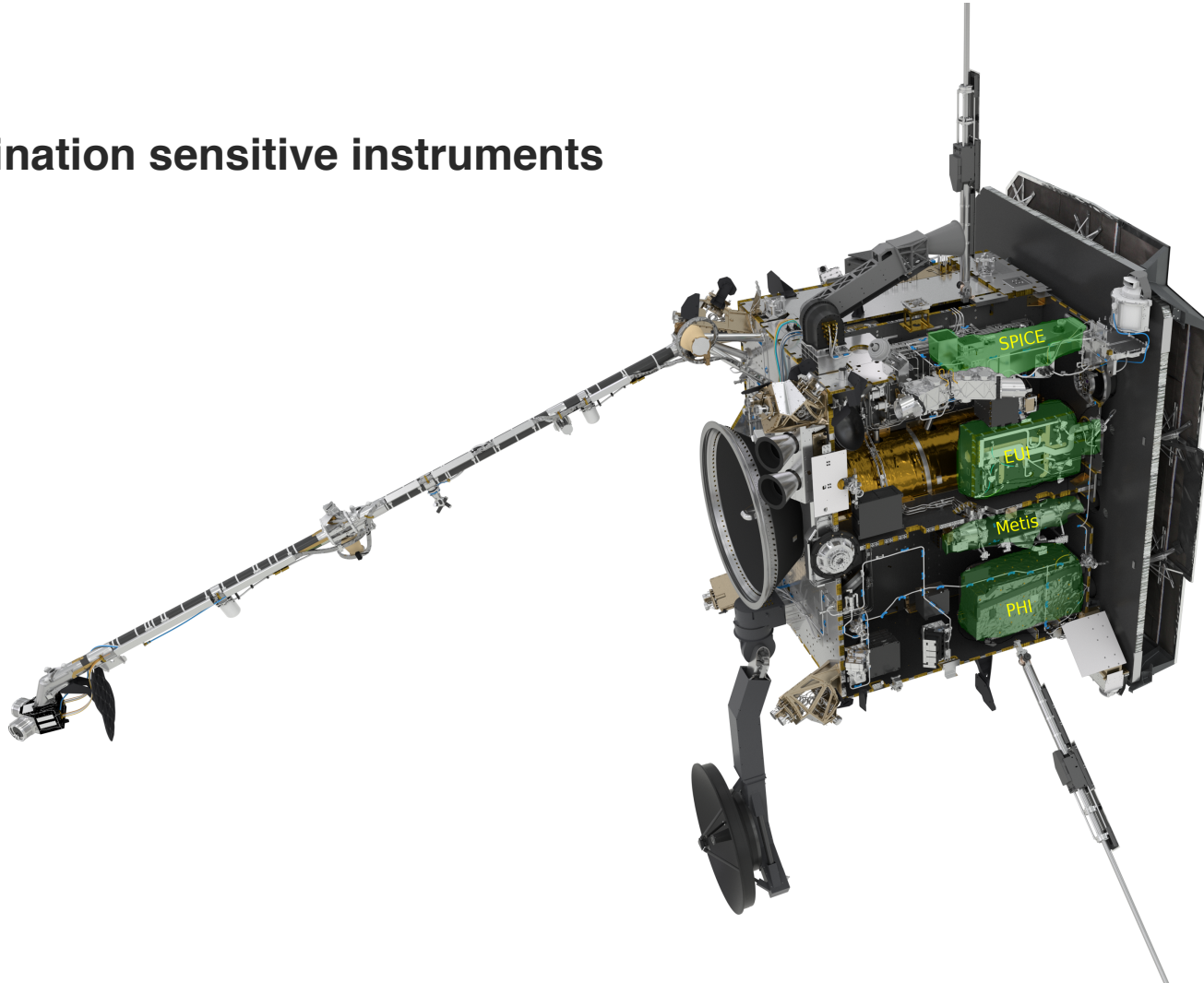
Solar Orbiter will make a **close approach** of the Sun **every six months**. Its distance from the Sun varies from within the orbit of Mercury to close to the orbit of Earth



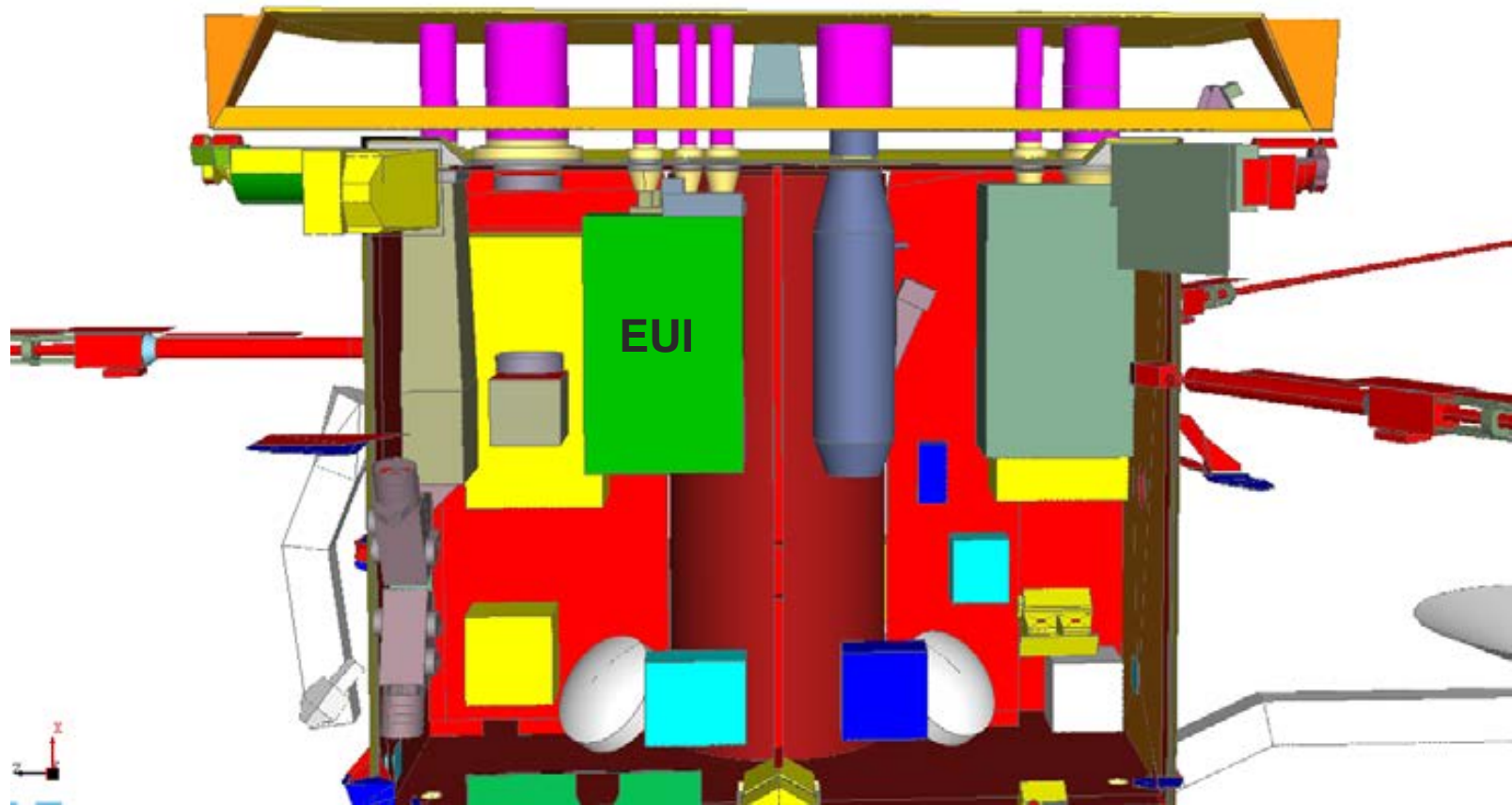
# Solar Orbiter S/C instruments



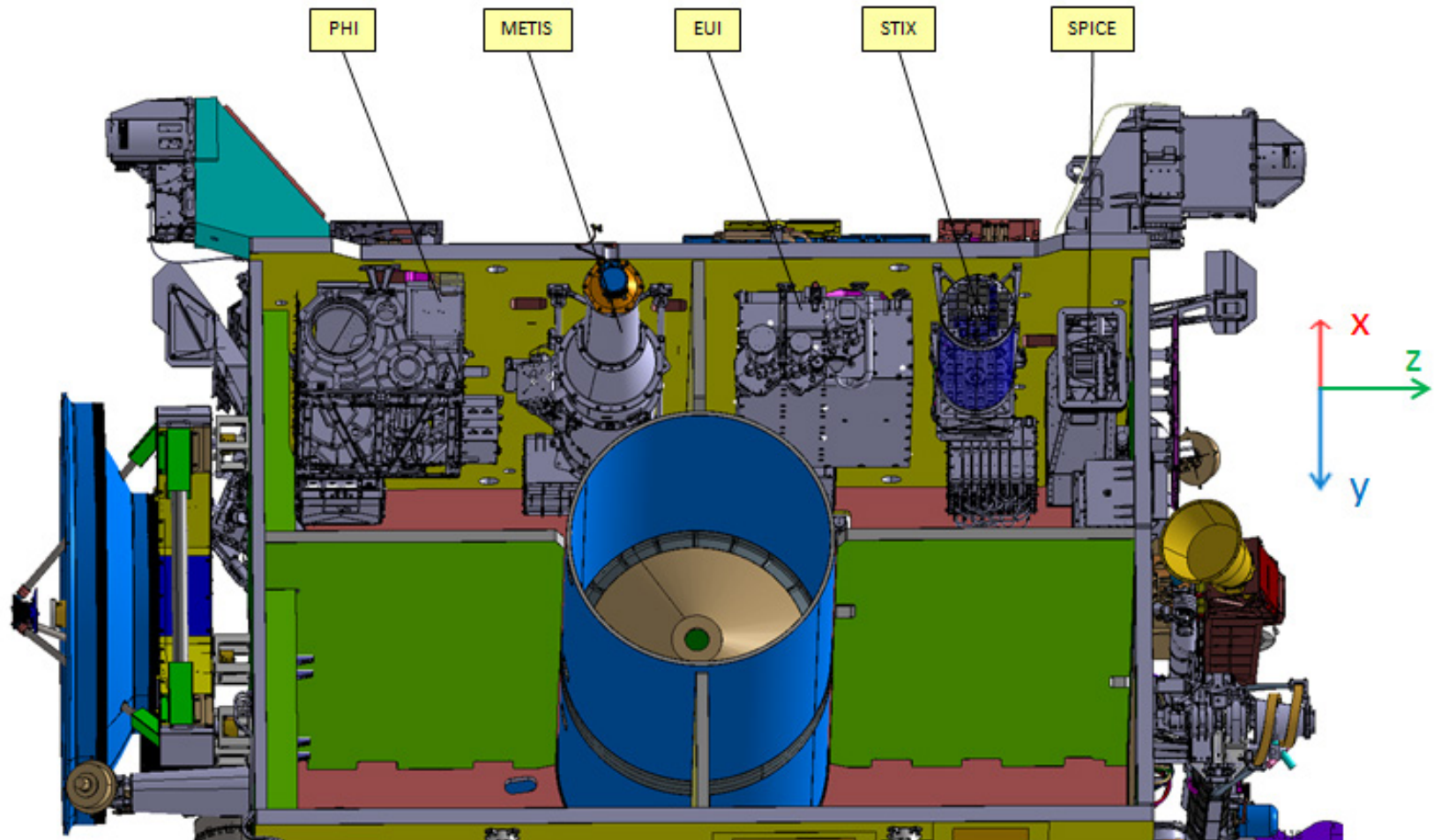
## Contamination sensitive instruments



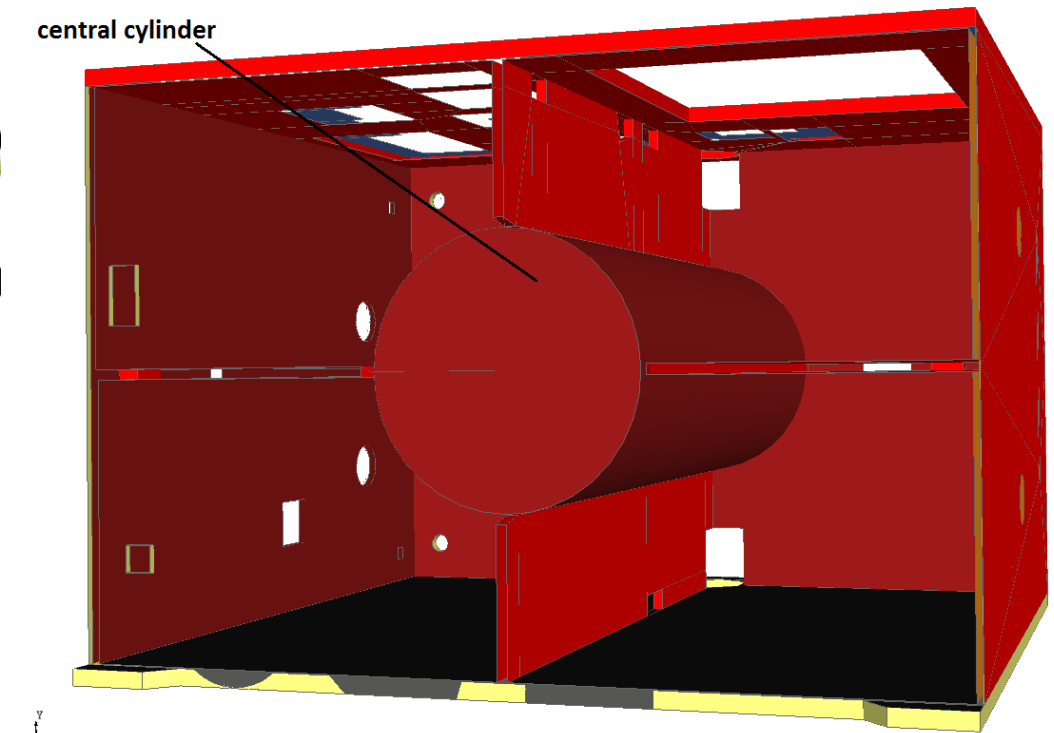
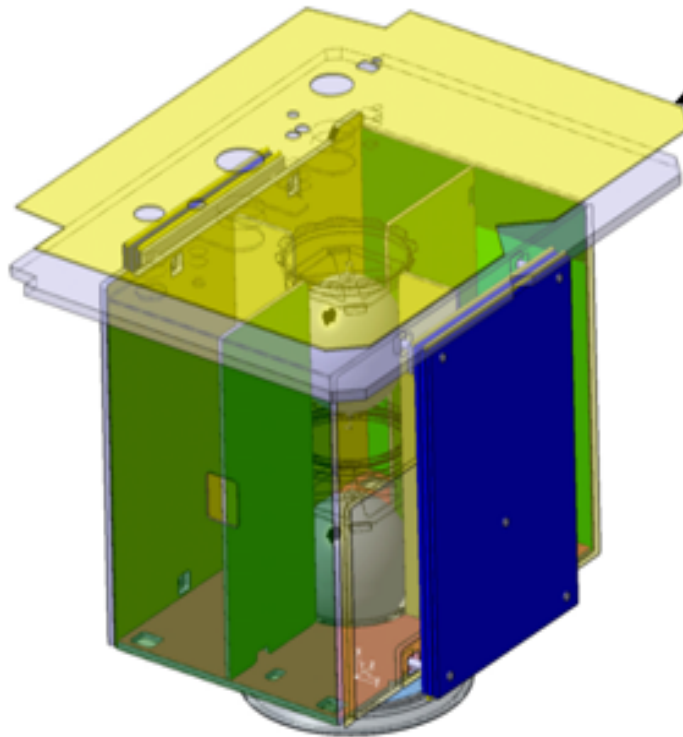
# Solar Orbiter Remote Sensing Instruments



# Solar Orbiter payload accommodation



# Spacecraft structure



4 quadrants with small venting holes

# In-flight contamination modelling



## 4.1.43 Contamination results for EUI\_EXT\_HW\_PY

During the considered mission time, the target 'EUI\_EXT\_HW\_PY' is subject to temperatures ranging from 273 K to 304 K with an average of 279 K. The EOL value for the total contamination (black dotted line) for this timespan is 20 577 ng/cm<sup>2</sup> with a maximum value of 45 708 ng/cm<sup>2</sup> occurring after 3 days, i.e., during the Pre-NMP. The main source material at the EOL is SOLO\_Harness\_int.

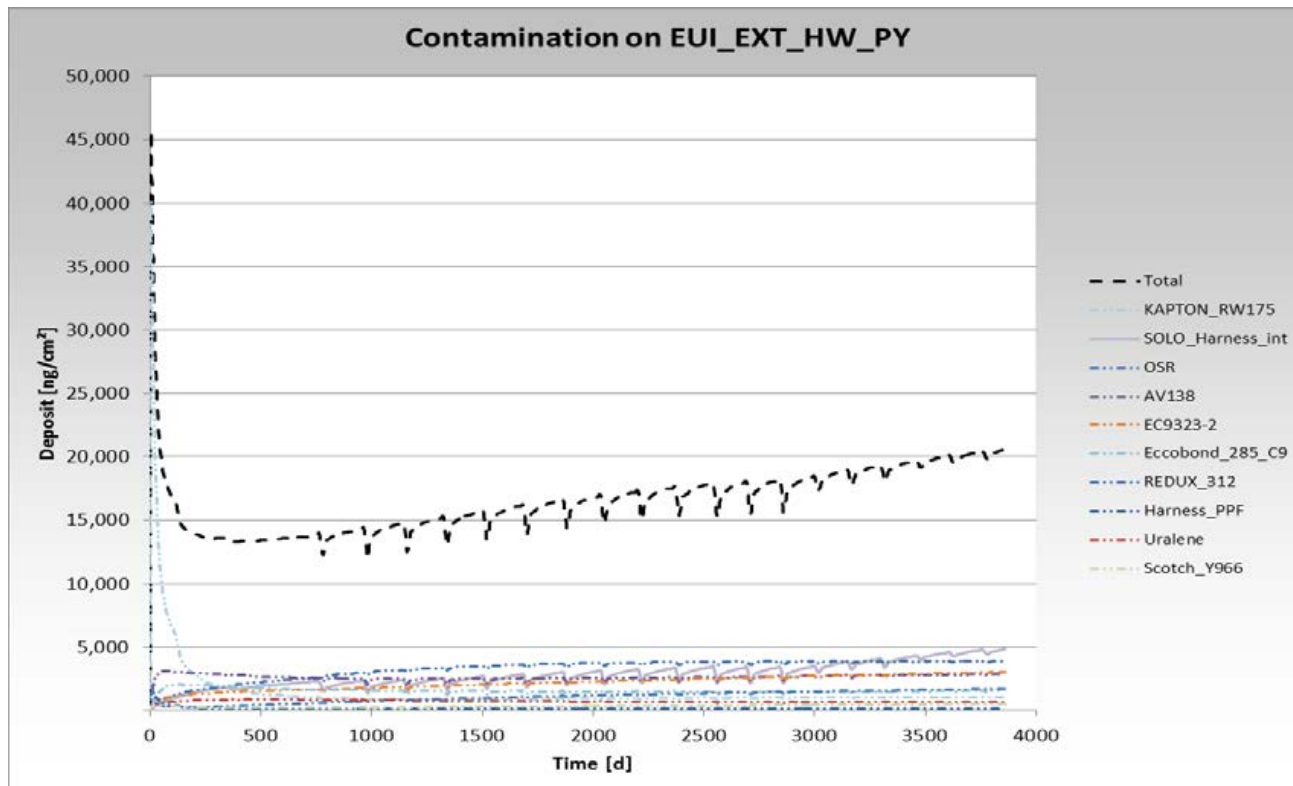
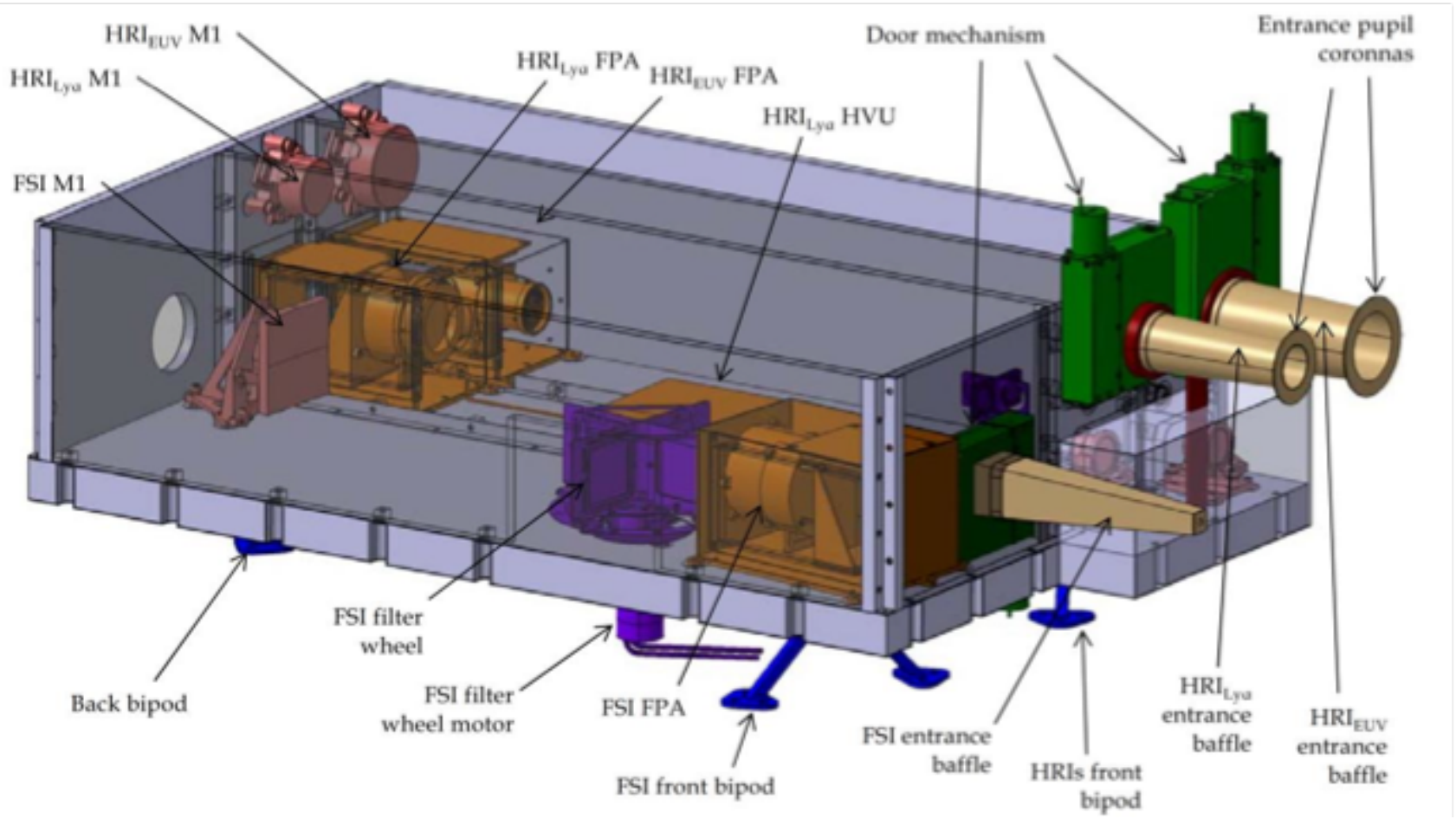


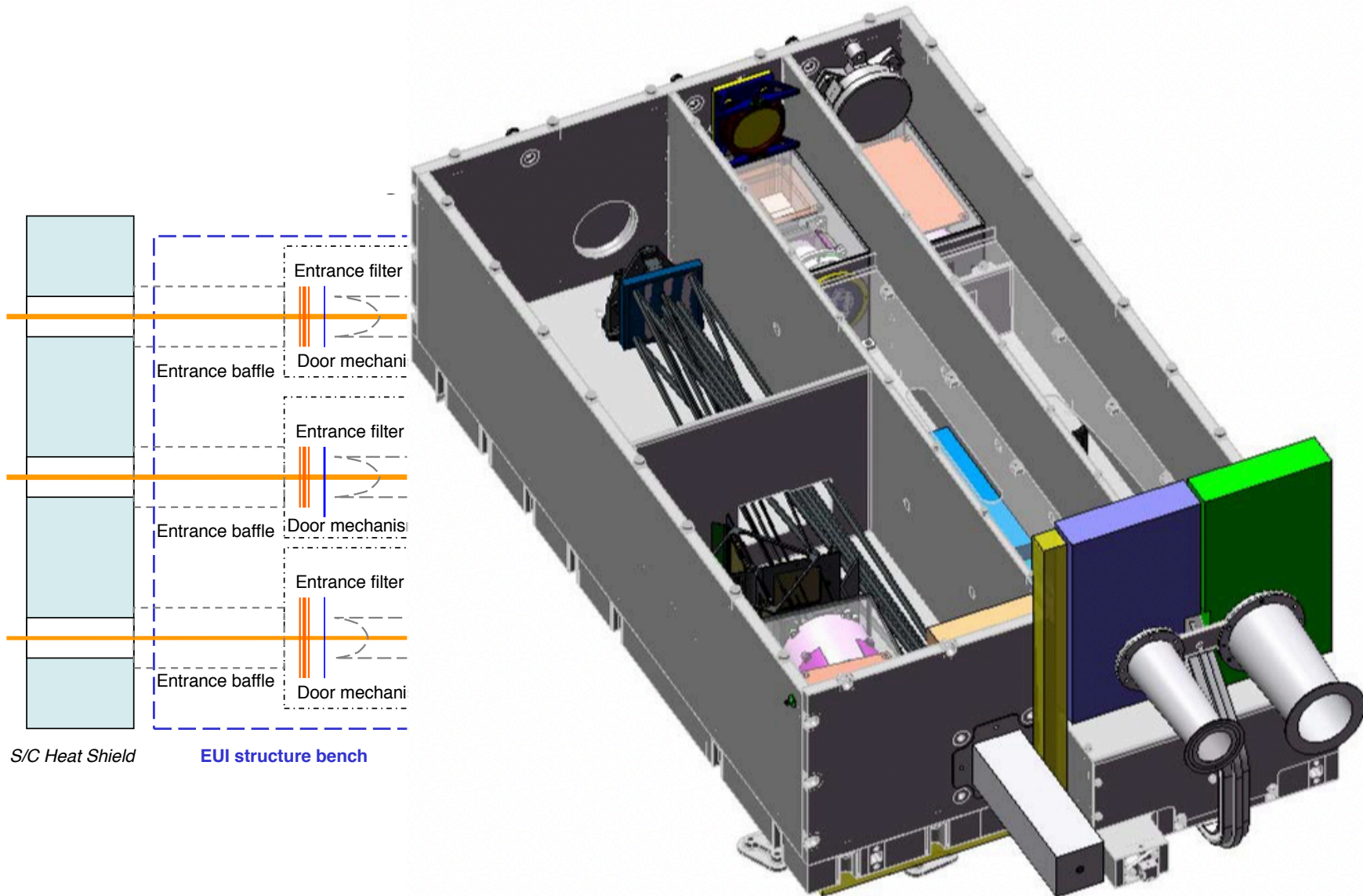
Figure 213: Contamination on EUI\_EXT\_HW\_PY.

# Instrument overview





# EUI Functional Diagramme



# EUI Calibration Concept

- Calibration of subsystems
- Calibration of the flight instrument

==> collaboration with PTB (Berlin)



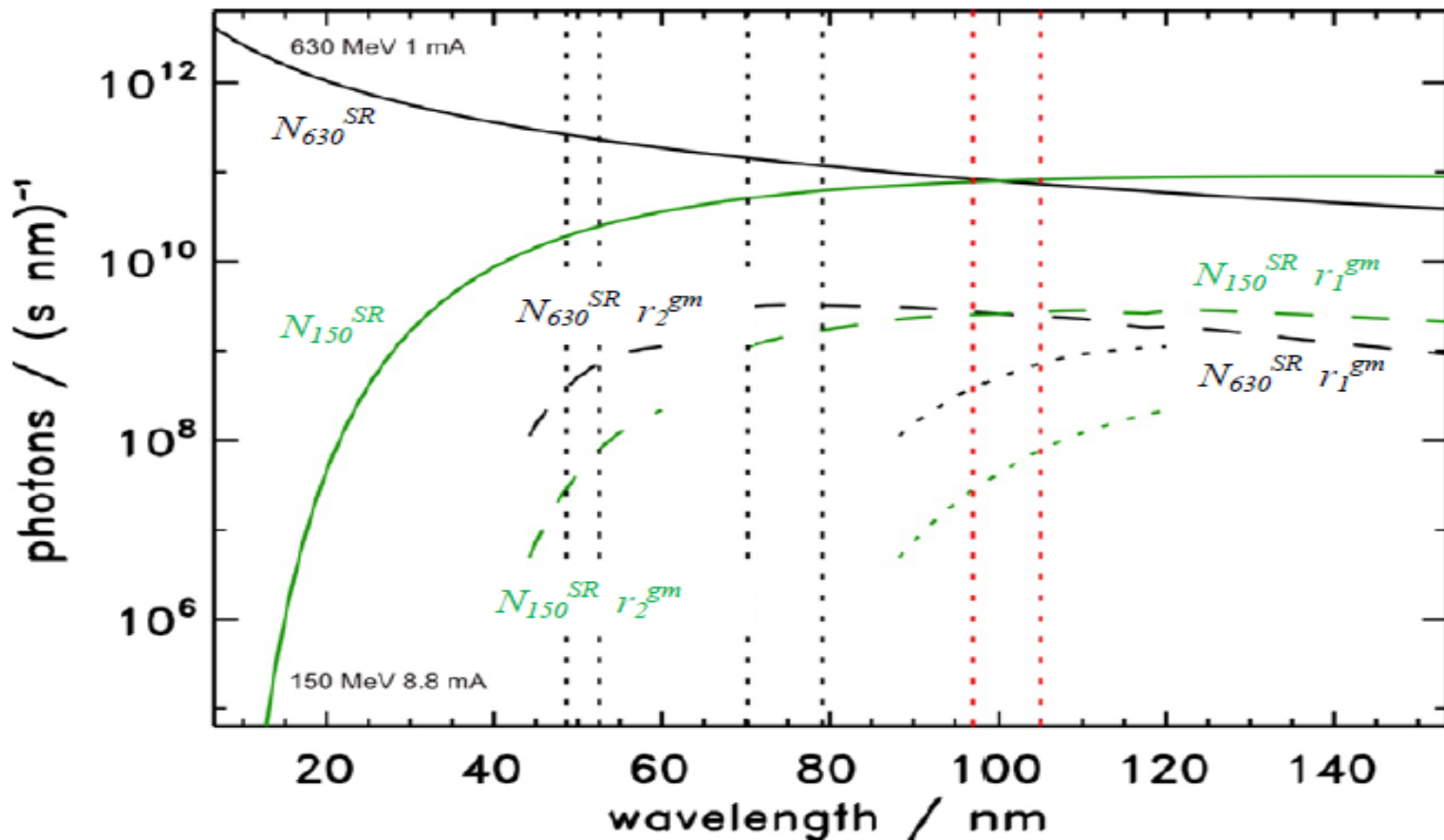
# Calibration of EUI subsystems



EUI Calibrations of Subsystems		
		FSI, HRI-EUV, HRI-Lya
<b>Filters</b>		Entrance filter + Focal filter
	Spectral Transmission	
	Uniformity at peak lambda	
<b>Mirrors</b>		Coating witness mirrors
	Spectral Reflectance	
	Uniformity at design lambda	
<b>Detectors</b>		QM, FM, FS
	Spectral Response	
	Out-of-band Response	
	Uniformity of Response	



- Primary source standard, calculable precise intensity
- special operation of electron storage ring
- Continuous wavelength spectrum



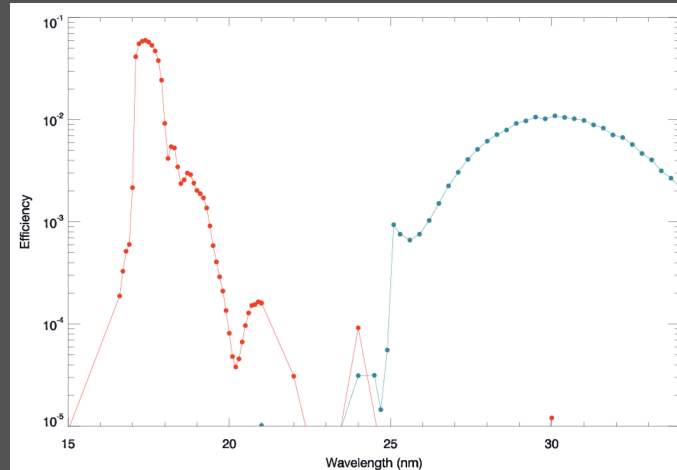




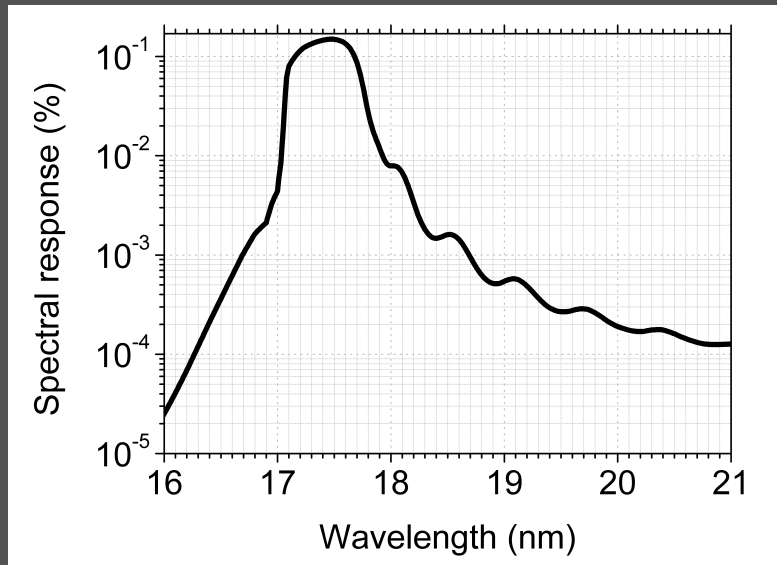
t the MLS calibration beamline



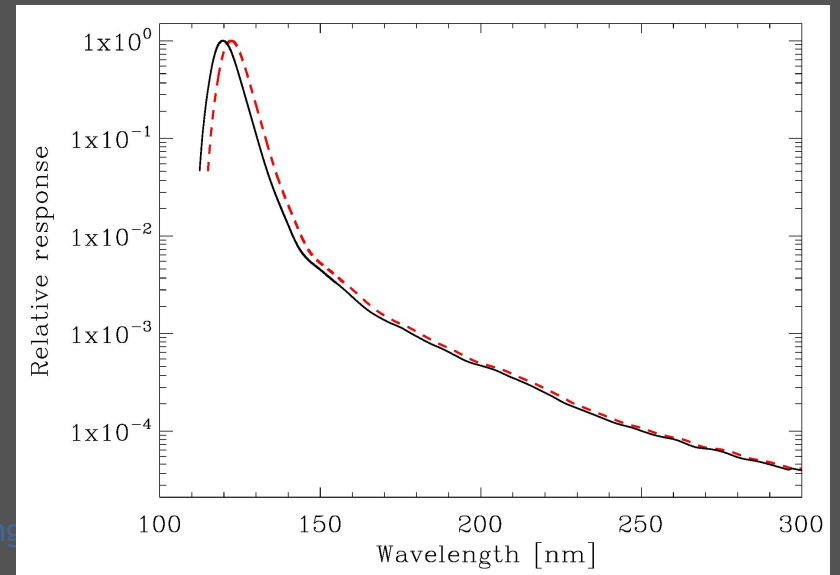
## Relative response of FSI



## Relative response of HRI EUV



## Relative response of HRI Ly $\alpha$



# EUI Cleanliness Concept

- keep degradation at a minimum
- keep calibration stability

==> design for cleanliness

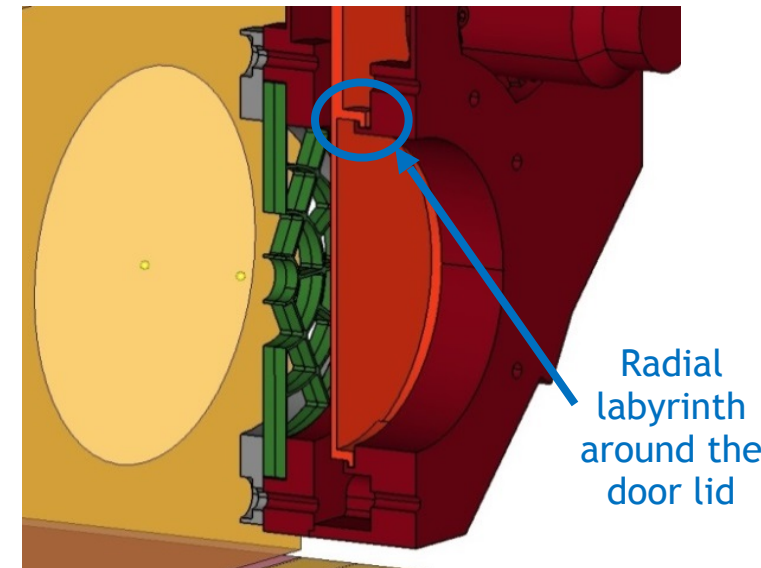
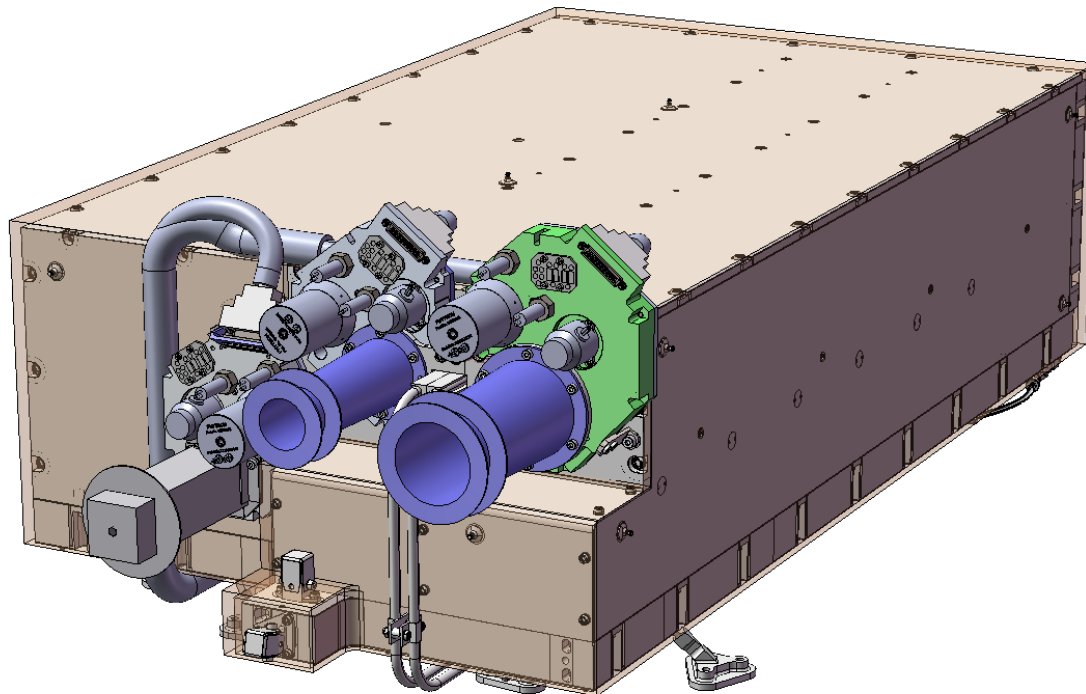


# EUI doors design



- New door design

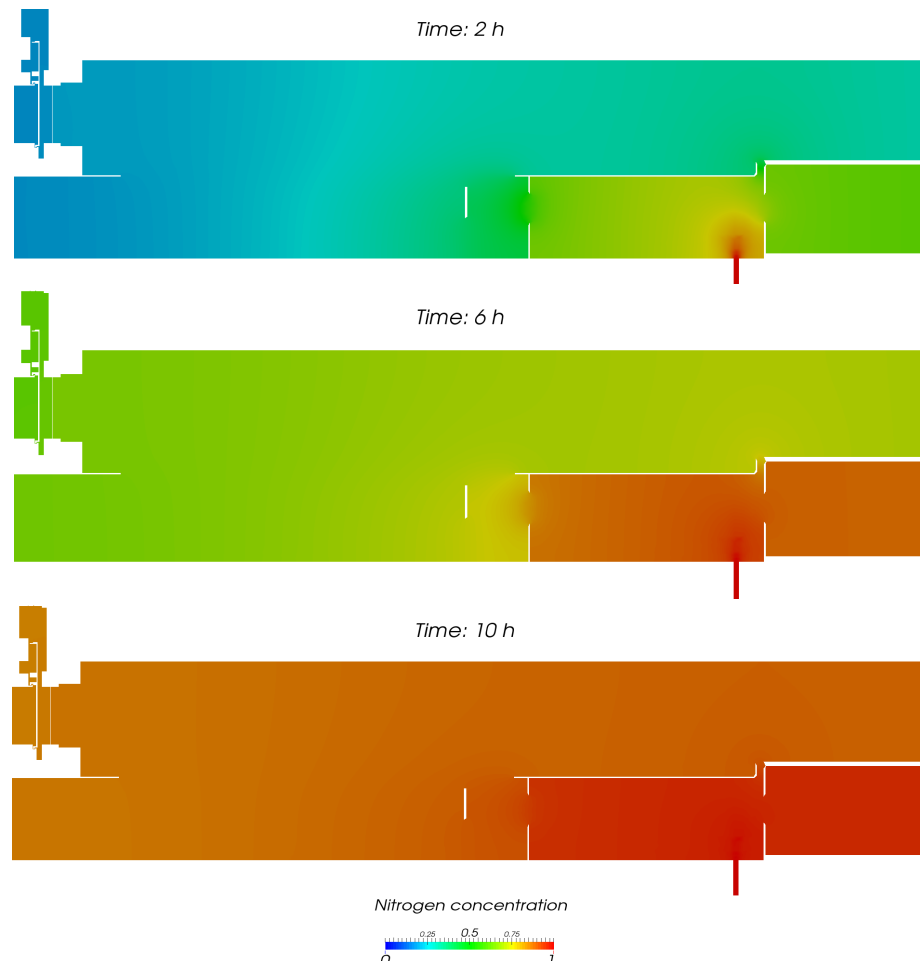
- Simpler mechanism → no sealing
- Labyrinths sized for depressurization and **purging** → purge rate increased to ensure positive  $\Delta P$  during purge
- NB: Interface with bench structure with GoreTex ring



# EUI design



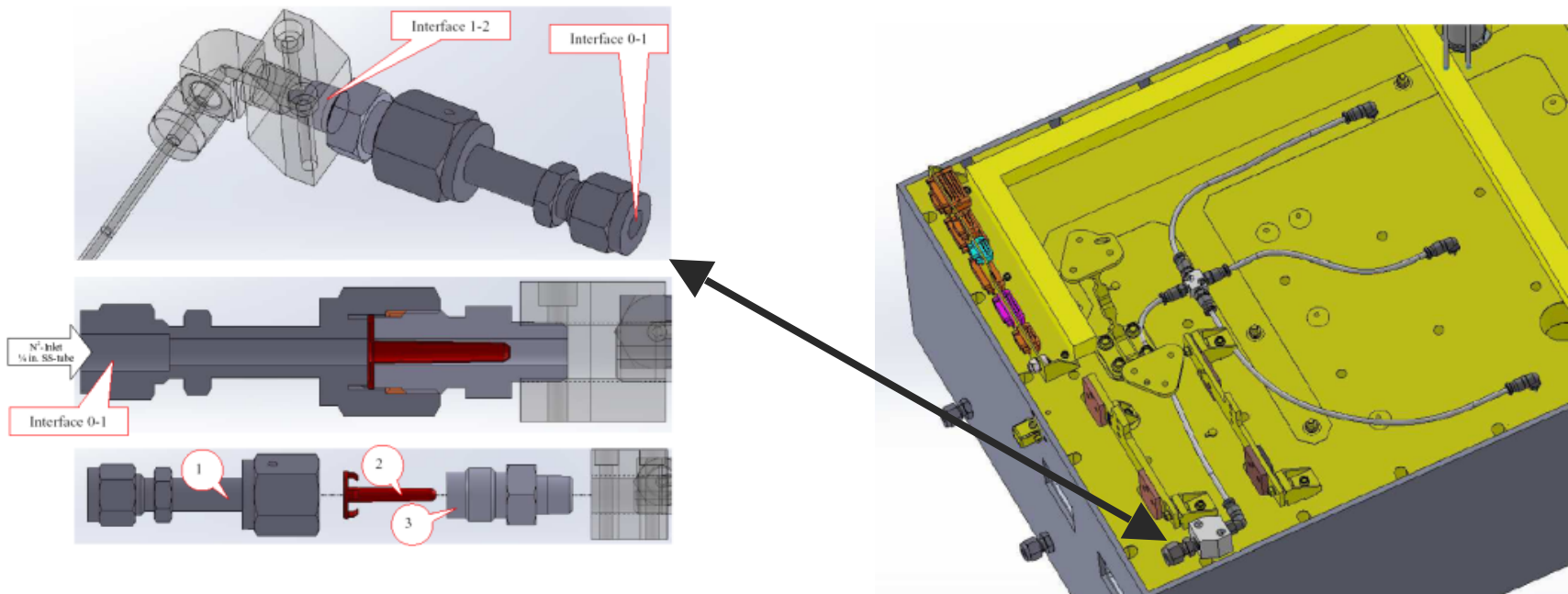
- Purge computation results



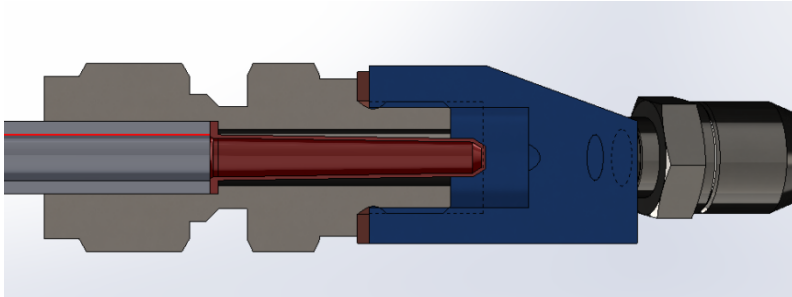
# EUI purge system design



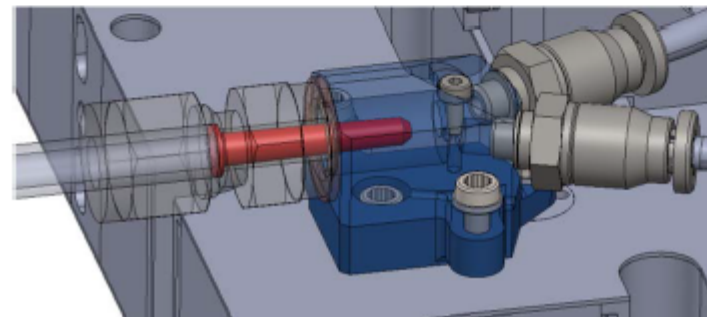
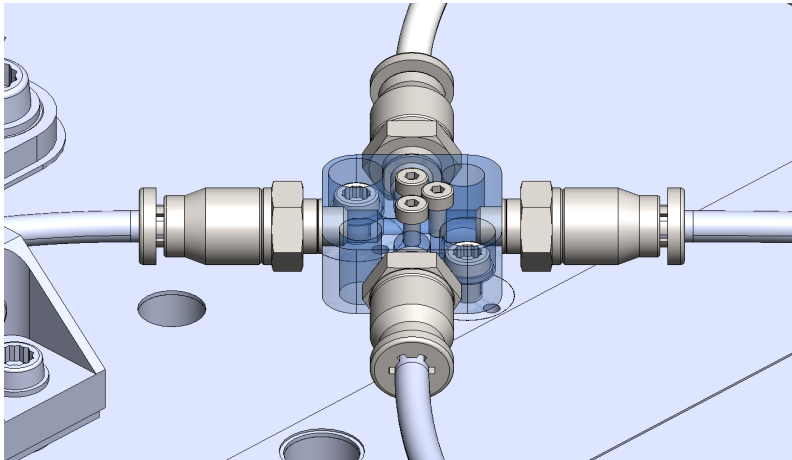
- Purge inlet interface
  - SS-400-1-4 to S/C
  - OBS external pipes for flow distribution to three channels



# Purge inlet filter and distribution



- Inlet particle filter  $\geq 0.4 \mu\text{m}$
- Teflon tubing
- Flow-rate adjustment with set-screws
- Total mean flow-rate = 2.56 liter/hr
  - $\text{HRI}_{\text{EUV}} \rightarrow 0.64 \text{ liter/hr}$
  - $\text{HRI}_{\text{Ly-}\alpha} \rightarrow 1.28 \text{ liter/hr}$
  - $\text{FSI} \rightarrow 2 \times 0.32 \text{ liter/hr}$

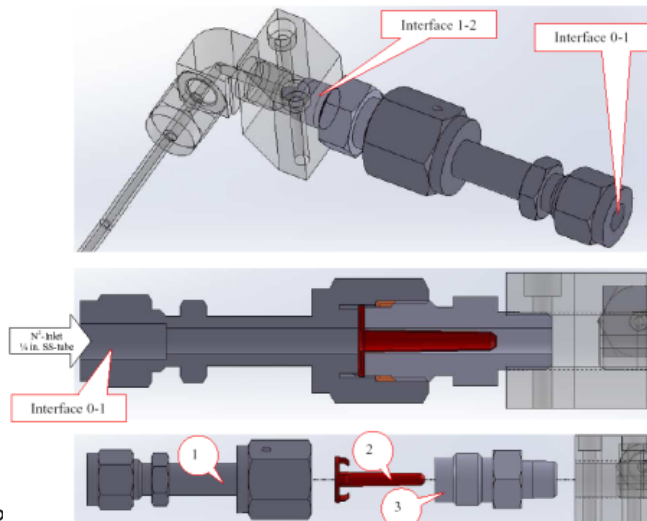


# Purge inlet & outlets

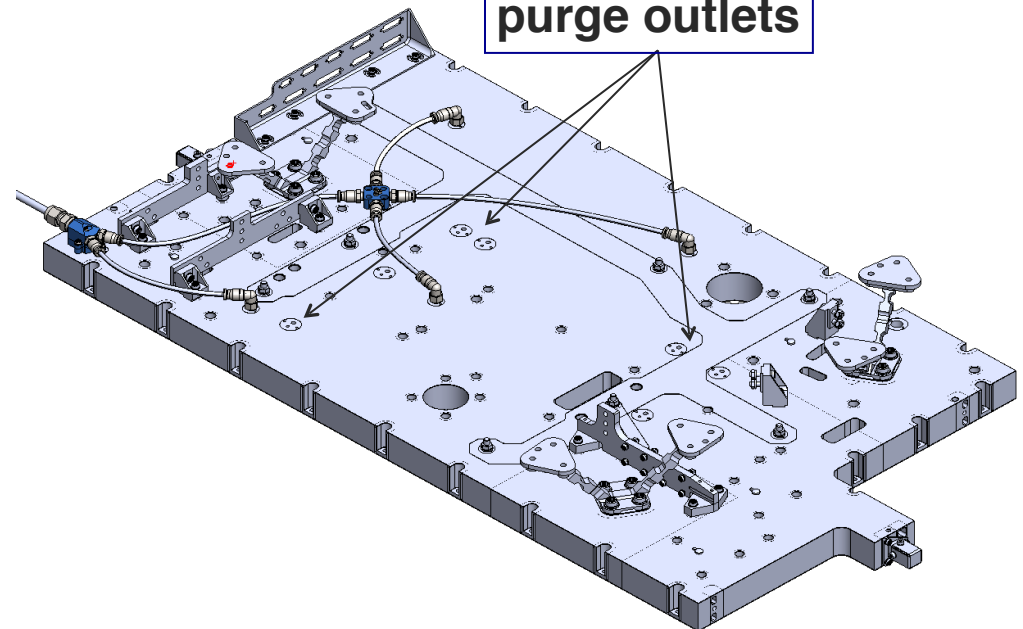


- purge interface Swagelock stainless steel model
  - EUI agrees to use SS-400-1-4 (smallest)
    - Only one inlet for the three channels and a dedicated piping system under bench (Swagelok/Festo parts)
    - Total flow rate is 12 – 80 l/h for the only inlet

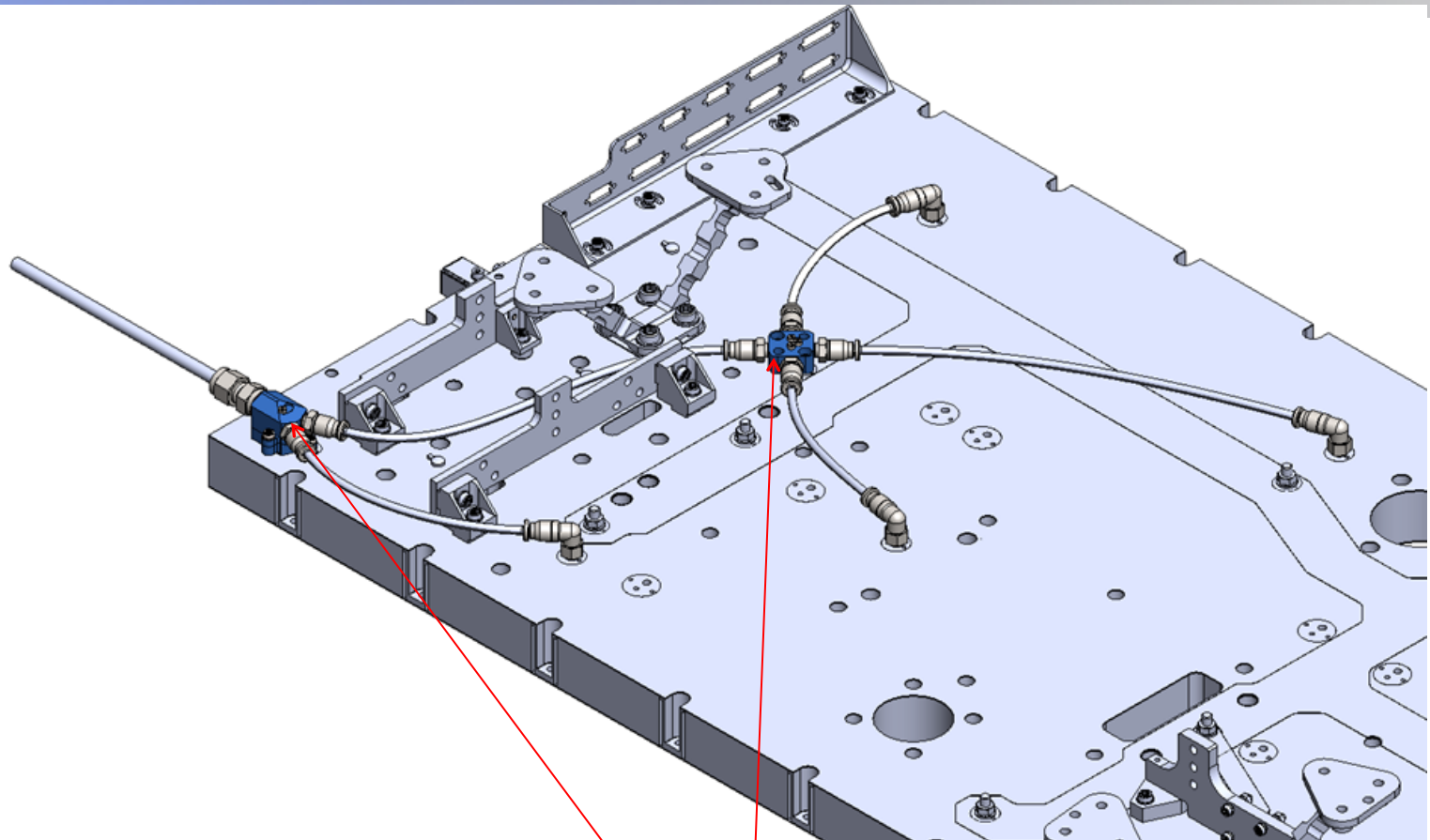
**purge inlet**



**purge outlets**



# Distribution of purge gas



Adjustment of the set-screws until following flow-rates are achieved:

- $HRI_{EUV}$  → 0.64 l/h
- $HRI_{Ly-\alpha}$  → 1.28 l/h
- FSI.1 → 0.32 l/h
- FSI.2 → 0.32 l/h

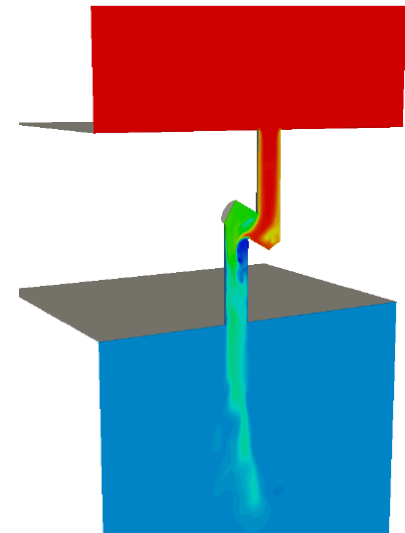
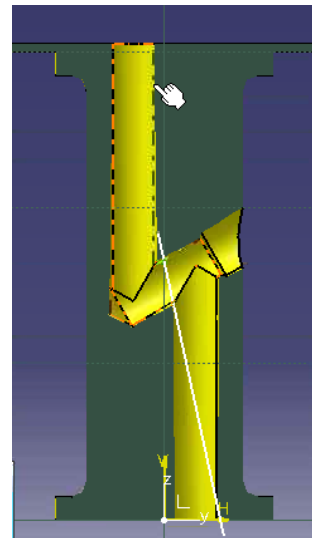
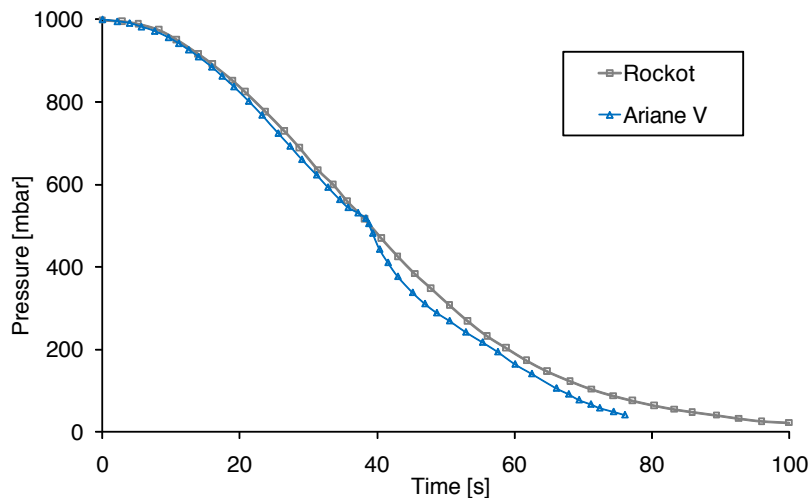
**Set screws to adjust individual flow rate**

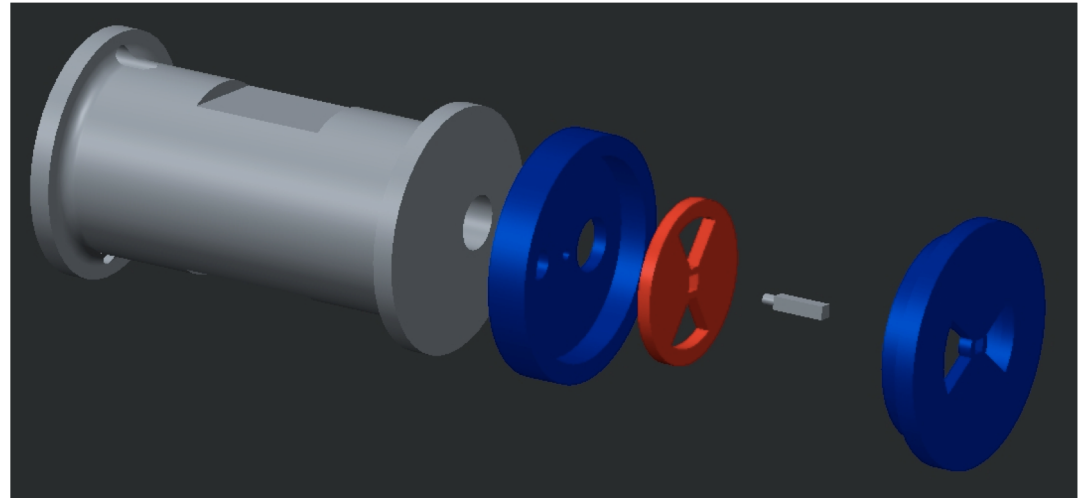
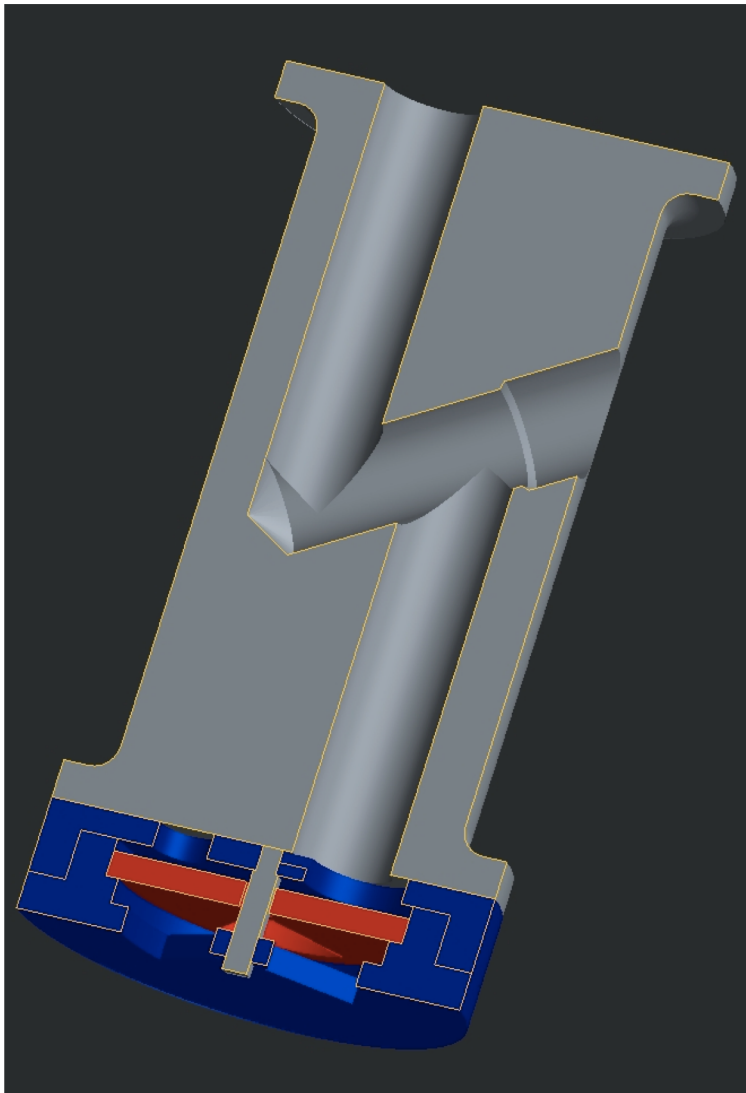
# EUI venting



## ■ Launch

- External pressure
  - 1 to 0 bar with peak of 6200 Pa/s
- Venting holes
  - 2 / 4 labyrinths in HRI / FSI channel
  - 2 mm<sup>2</sup> venting cross-section per litre volume 2 outlet per channel (drilled in dedicated inserts)







# EUI design update



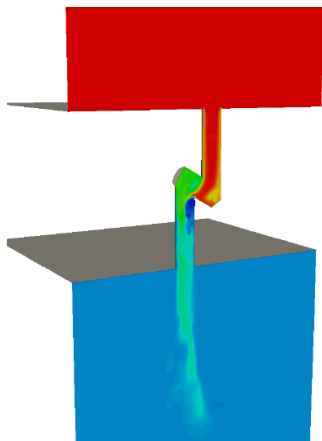
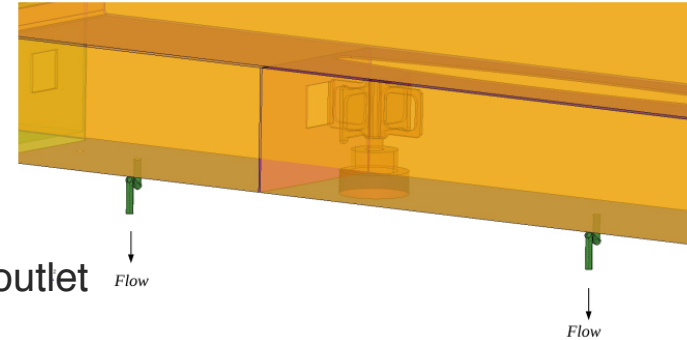
## ■ New door design

### ○ Door labyrinth sizing

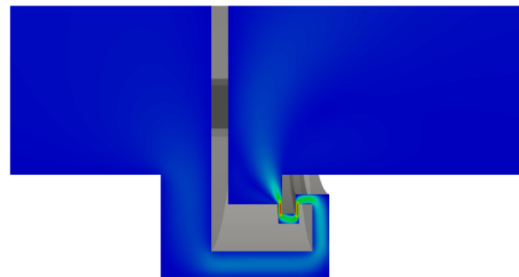
- 2 venting outlet in the bench
- door labyrinth ⇔ one additional venting outlet

### ○ CFD analysis

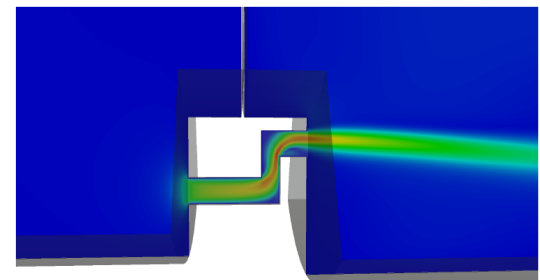
- ➔ Limited  $\Delta P$  around entrance filters ( $< 2$  mbar) during launch and purging
- ➔ Overpressure (0.001 mbar) during purging (compromise with launch venting)
- ➔ Few hours to fill cavity with  $N_2$  ( $> 80\%$  in 10 hours)



Venting outlet head loss coefficient computation



Door labyrinth head loss coefficient computation

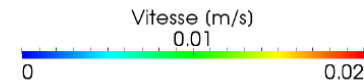
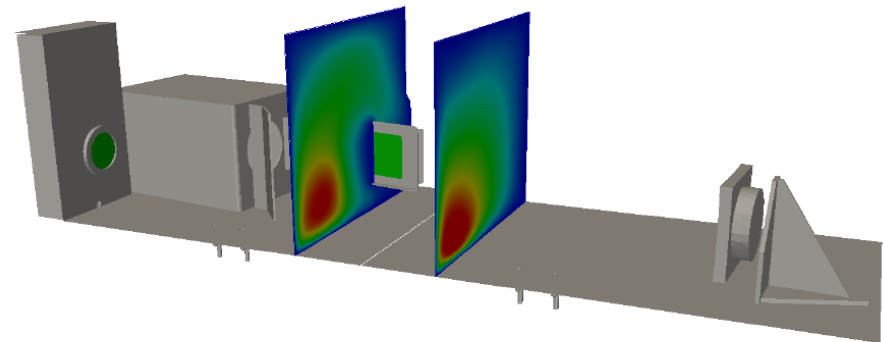
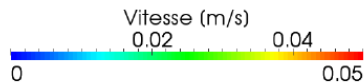
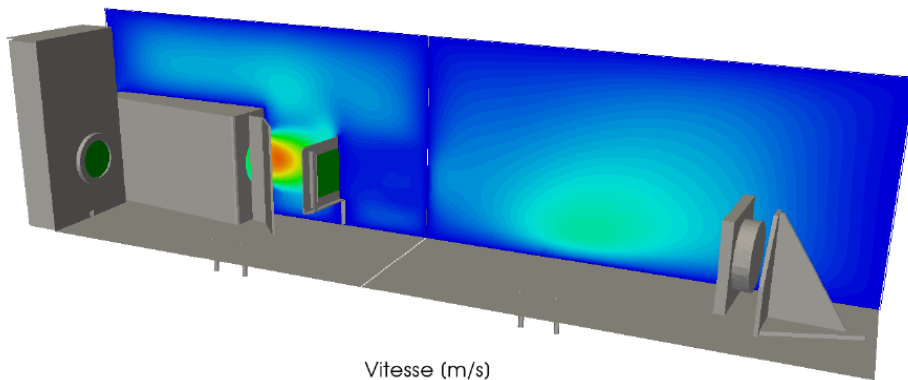
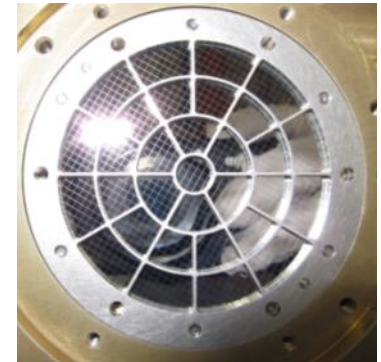
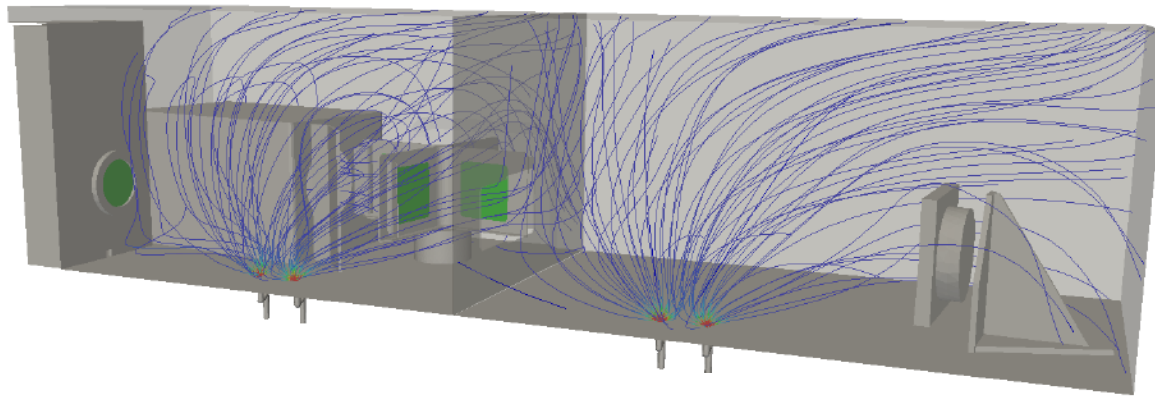


Filter labyrinth head loss coefficient computation

# EUI venting simulation



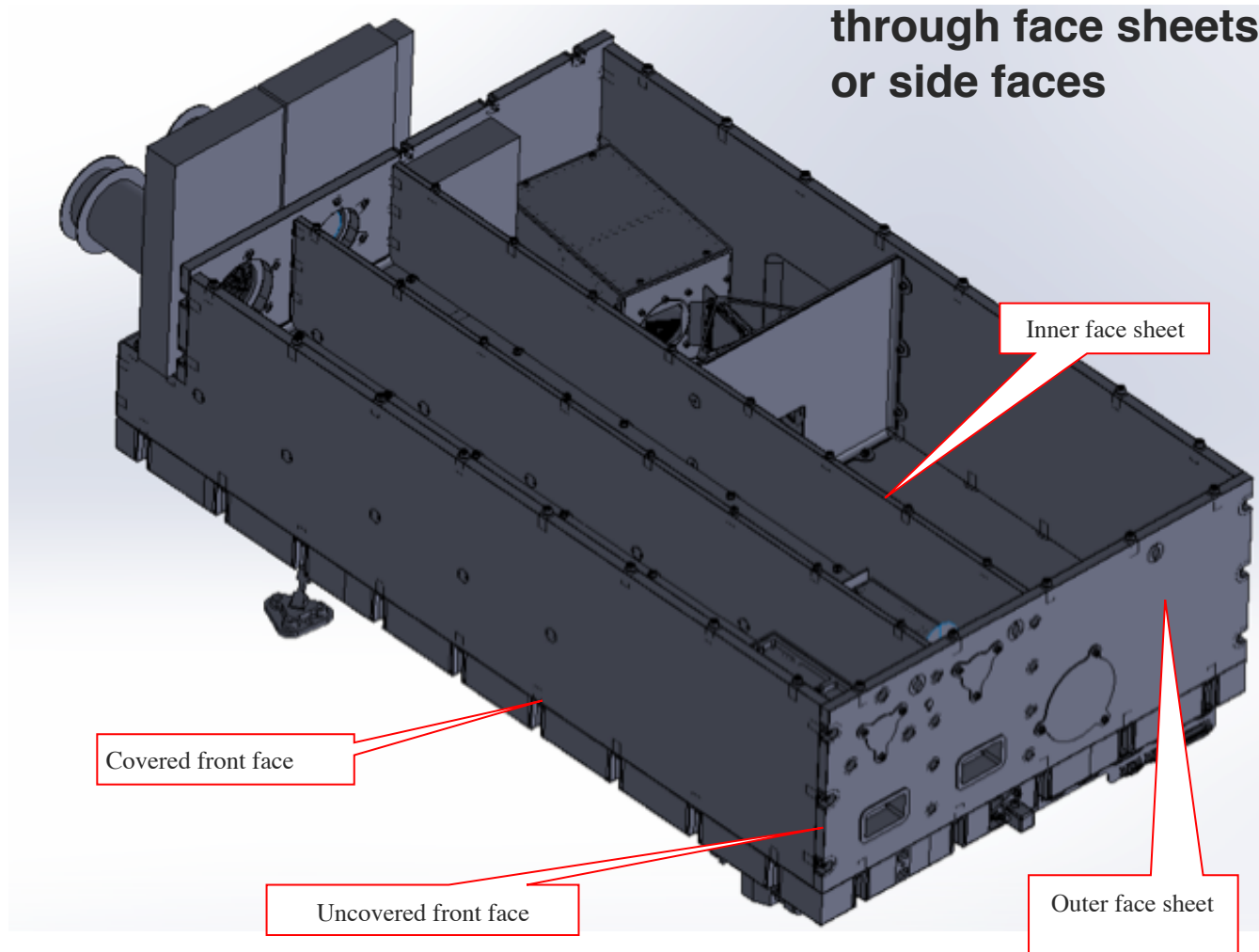
- Launch
  - Impact on filters
    - $\Delta P$  around filter wheel and entrance filter  $\ll$  1mbar



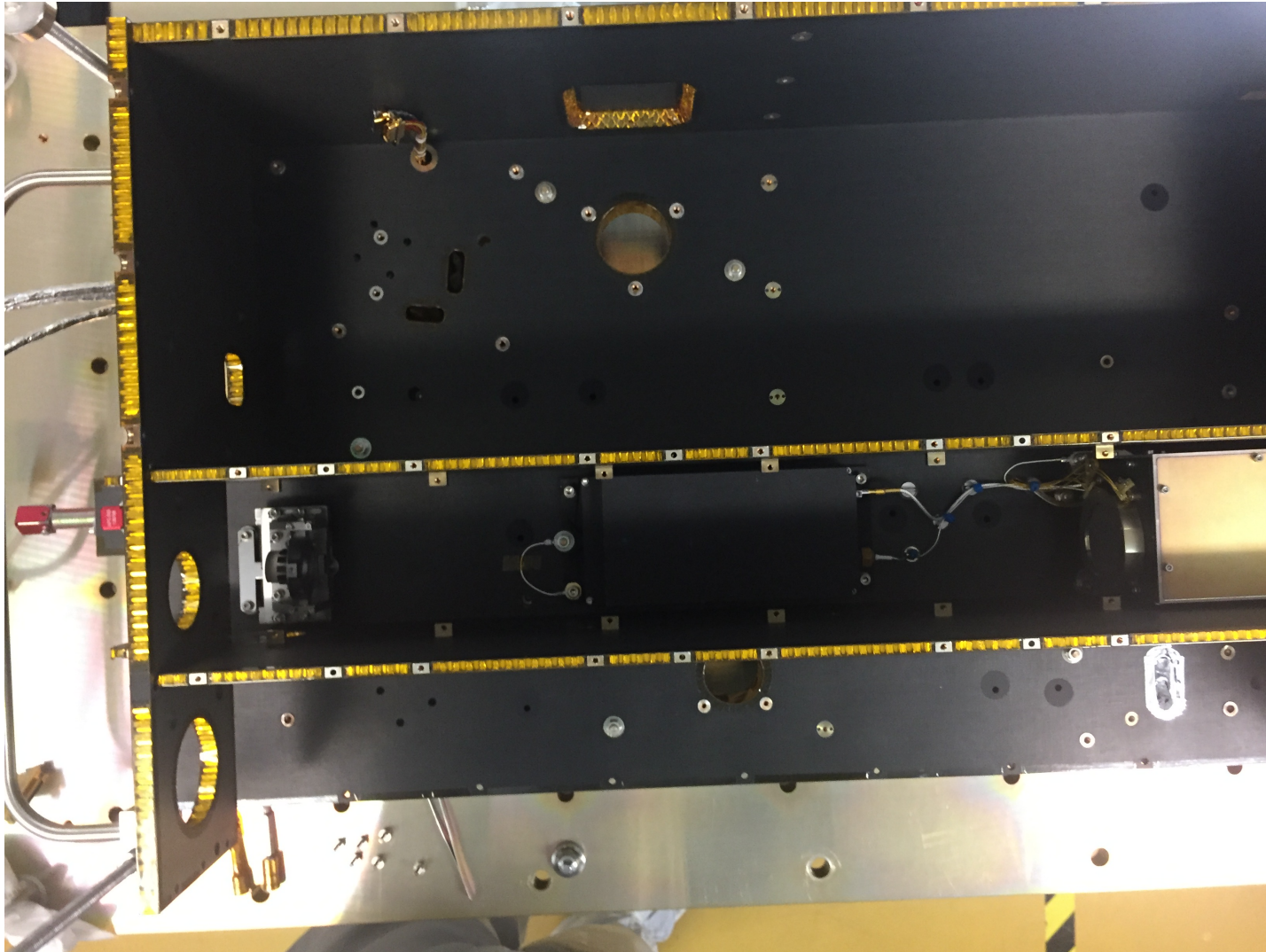
# Venting of CFRP structure panels



Venting under the MLI:  
through face sheets  
or side faces



# Venting of CFRP structure panels

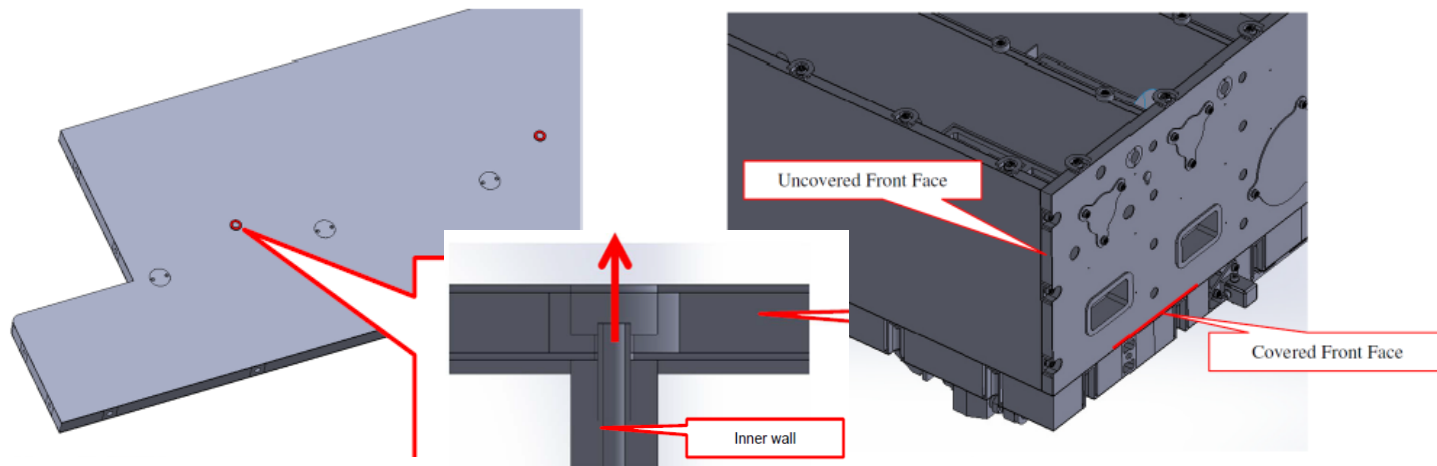


# Venting of CFRP panels



## Venting – External panels

- venting inserts on outer faces
- perforated Kapton tape on open side faces
- venting of internal panels through top panel

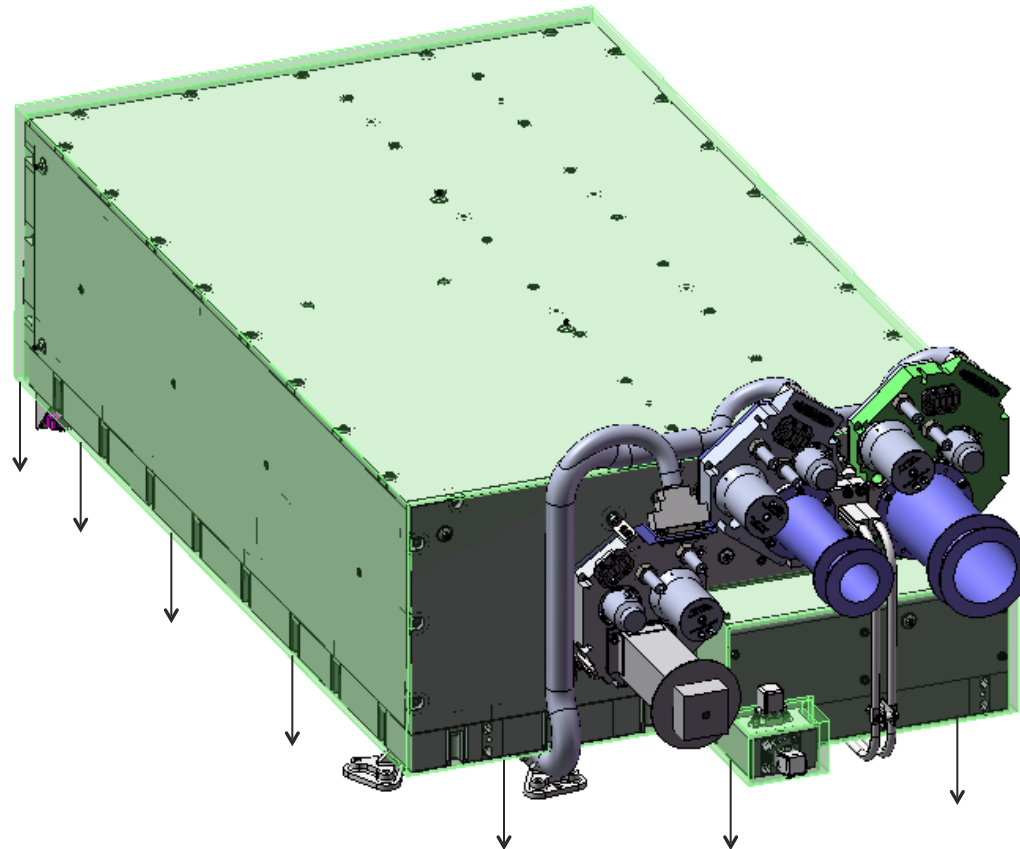


# MLI venting

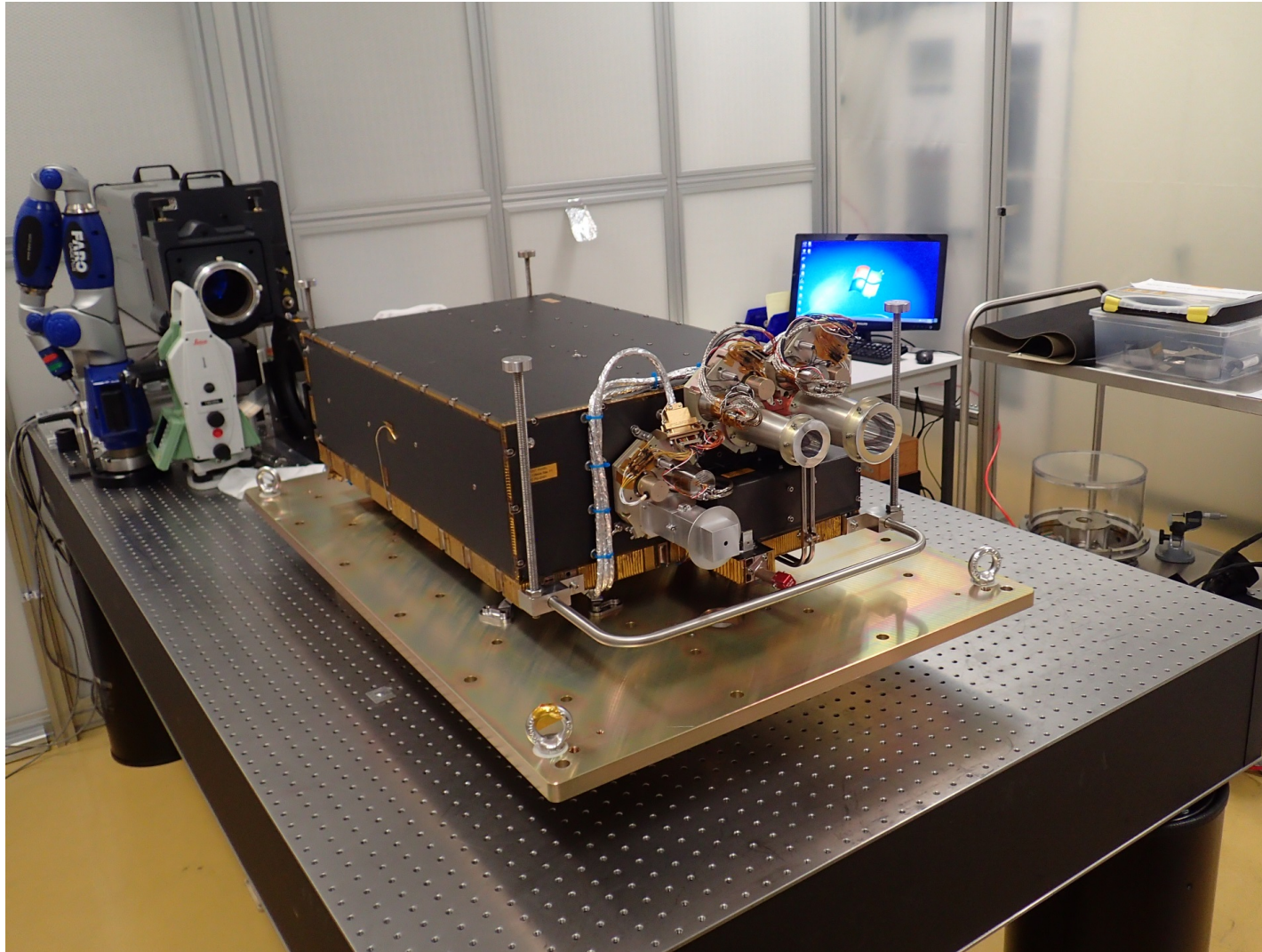


- EUI OBS MLI

= 2 layers of Mylar → no micro-perforation → venting by bottom part, around unit), as per on STM



# CFRP housing structure



# EUI purging requirements



## ■ EID-B requirements

- The prime contractor shall ensure after EUI delivery almost continuous purging of the EUI structural housing with clean and dry nitrogen gas until launch.
- The longest duration **without purging shall be limited to 30 minutes per any 24 hours**, except during the vacuum tests sequences. ==> was extended to 60 minutes by Prime request.
- The Prime Contractor shall purge EUI, after delivery, with **gas quality grade 5.0**, i.e., 99.999% vol N<sub>2</sub>, <3 ppm O<sub>2</sub>, <5 ppm H<sub>2</sub>O, < 0.5 ppm hydrocarbons. Synthetic air of the same quality may be used. Before delivery, gas quality used will be Grade 6.0 (or BIP 5.2) ==> was changed to MIL-PRF Grade C quality by prime.
- The purging **flow rate shall be in the range 12 – 80 l/h**. ==> was implemented by flow restrictive capillary.
- **The maximum purge pressure spike shall be 0.003 bar**. ==> changed to 30 mbar/minute
- The purge shall be maintained with a log of all purge interruptions.
- During AIV of the spacecraft and on the launcher inside the fairing a gas supply is required to sustain a flow rate in the range 12 – 80 l/h.
- The Prime Contractor shall ensure that after re-pressurisation of vacuum chamber, the clean gas is supplied through the purge inlet connector on the spacecraft. ==> changed to a slight overpressure to be maintained.  

NB: during vacuum chamber repressurization, the purging system can be used but shall not be the only source of re-pressurization. If used, the purge flow shall be controlled to have a maximum of 0.5 l/h. ==> changed to 12 l/h.
- The spacecraft test plan shall not include a specific opening of the internal EUI-OBS doors, except when under vacuum. ==> changed to never opening.

◆ **Purging during flight to the launcher to be maintained**

◆ **Purging on the launcher to be maintained**

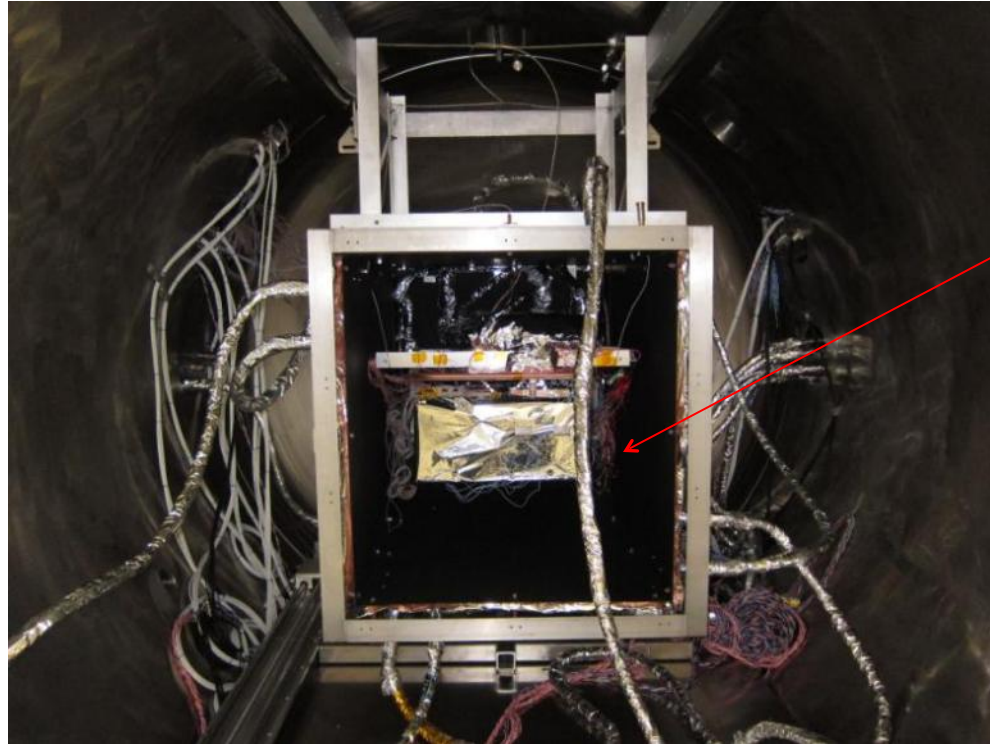


# EUI cleanliness monitoring

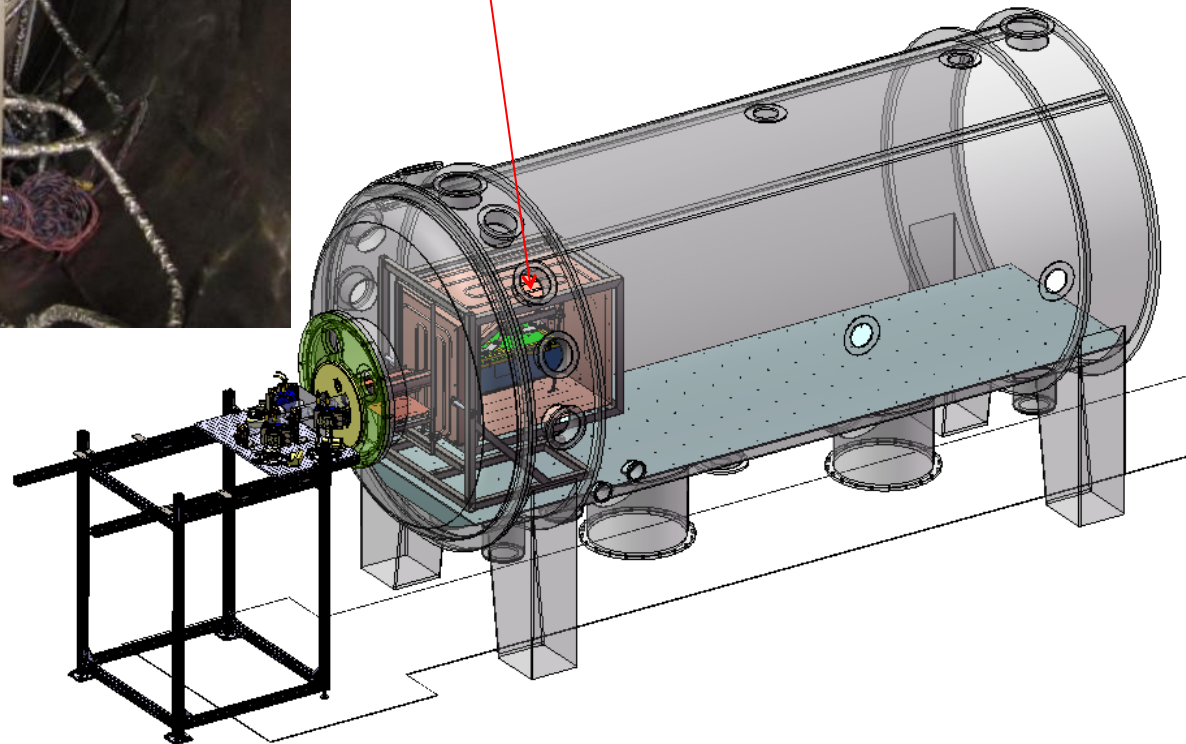


- Particular and molecular witness samples
  - Will follow the unit all along its AIT activity
  - Allows cleanliness monitoring (after assembly, vibration, vacuum/bakeout tests...)
  - Some witness samples also on S/C MY panel during AIT
- Types of witness samples
  - Particular:
    - PFO
    - Monitored @CSL
  - Molecular:
    - Metallic witness plates (ECSS Q-70-05C – indirect method)
    - Monitored by FTIR @CSL

# EUI vacuum tests



OBS STM unit in vacuum chamber



# Vacuum thermal bake out



- Bake out with monitoring by RGA, witness plates and
- Temperature-controlled Quarz- Crystal Microbalance TQCM
- with SUCCESS CRITERION:
  - monitor the TQCM frequency  $f$  / Hz
  - until rate of change of frequency  $f''$  /Hz/h/h is  $< 1\%$

# Bake out analysis



## 8.2. TQCM criteria

The TQCM record over the bakeout is shown in next figure.

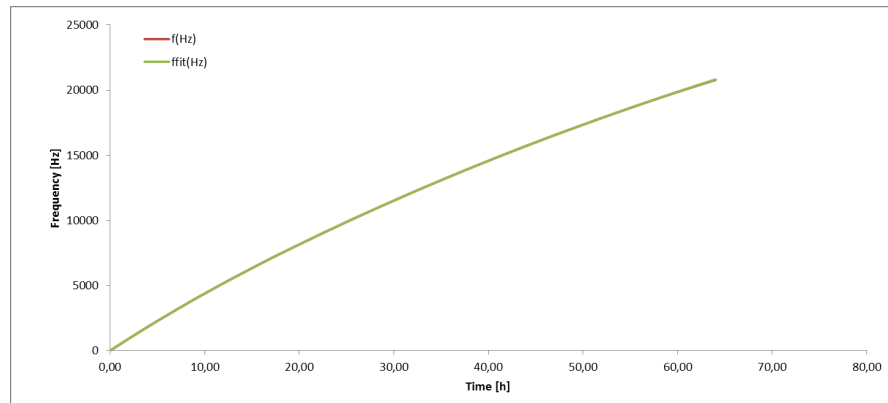


Figure 8-2: EUI FM cameras bakeout - TQCM frequency record

The deviation of linearity ( $f''/f'$ ) success criterion is shown in next figure, and is lower than 1% at end of bakeout.

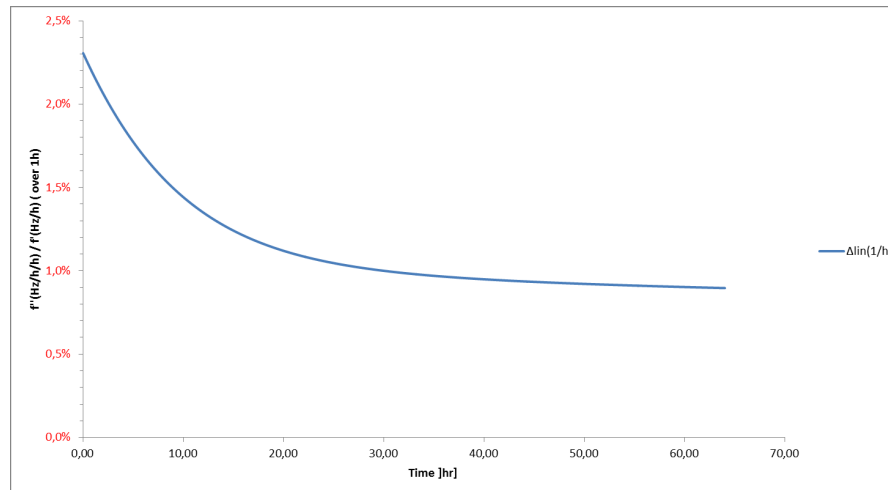
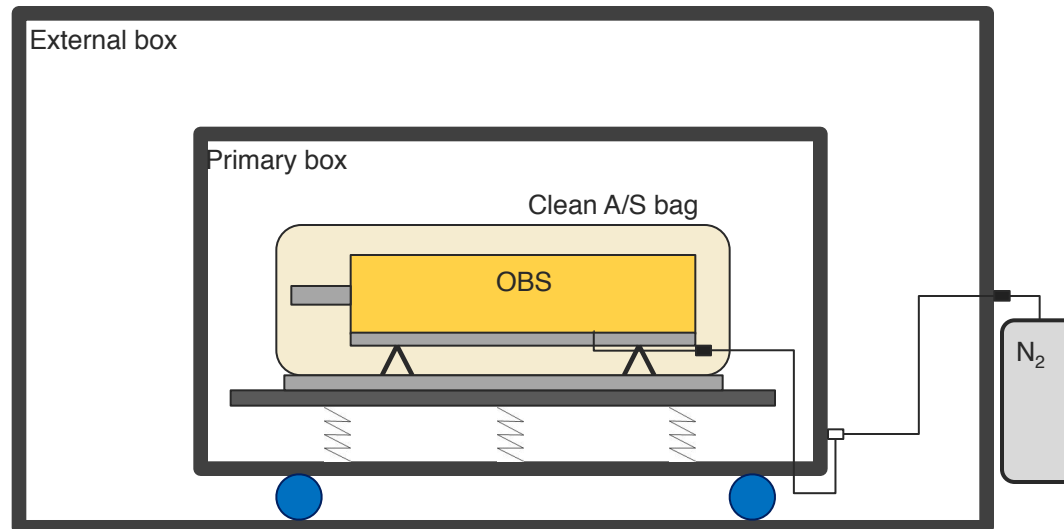


Figure 8-3: EUI FM cameras bakeout - $\Delta\text{lin}(1/h)$  using fitted TQCM data

# EUI OBS transport container



- Inner ('primary box') and outer ('external box') containers
  - OBS wrapped in clean anti-static bag, and fixed on a transport plate in the primary box
  - Primary box on a damping system in the external container
  - External box equipped with purging system for primary box (same inlet interface SS-400-1-4 than in OBS)



# EUI OBS transport container



- Primary box

- It can be use in clean room class 100.
- It is equipped with a breathing valve, a desiccant box and a humidity indicator to provide the ambient environment.
- The breathing valve regulates the pressure inside the primary box at  $\pm 17$  mbar.

- Secondary box

- It an be use in clean room class 100.000.
- It is equipped with monitoring of humidity, temperature and pressure.

# EUI OBS transport container



- Outer container



# EUI OBS transport container



- With STM unit





# S/C transportation and launch site activities



## ◆ Purging during flight to the launcher to be maintained

- was major concern because of re-pressurization of airplane during decent.
- Antonov aircraft takes 10 minutes decent phase. makes 100 mbar over-pressure possible inside container.

## ◆ Purging on the launcher to be maintained

# Acknowledgements



- Solar Orbiter Mission: ESA
- Spacecraft: Airbus D&S
- EUI instrument: CSL, MSSL, IAS, PMOD/WRC, MPS